PASSPORT PARK

DRAINAGE MASTER PLAN

IRVING, TARRANT COUNTY, TEXAS





October 18, 2017

TX REG. ENGINEERING FIRM F-14439 TX REG. SURVEYING FIRM 10193805 7557 RAMBLER ROAD SUITE 1400 DALLAS, TX 75231-2388



BIG BEAR CREEK CITY OF IRVING, DALLAS COUNTY, TEXAS

PREPARED FOR:

F.A. PEINADO, LLC



PREPARED BY:



TX REG. ENGINEERING FIRM F-14439 TX REG. SURVEYING FIRM LS-10193805 PK NO: 1469-17.026

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EXECUTIVE SUMMARY

Pacheco Koch was retained by F.A. Peinado, LLC. on behalf of Bandera Ventures to prepare a site development drainage master plan associated with Passport Park which is an industrial development within the DFW Airport. The project is located northeast of the intersection of International Parkway and State Highway 183 in the City of Irving, Texas.

The purpose of this analysis is to develop a drainage master plan for the proposed Passport Park industrial development. This master plan defines detention requirements for the proposed development area. The detention requirements were developed by comparing pre- and post-project conditions for the 1-year, 25-year and 100-year storm events as outlined in the ISWM Criteria Manual, 2015. Existing 100-year floodplain inundation limits for three minor tributaries within the proposed development were defined. It is anticipated that a detailed floodplain reclamation plan and detailed detention configuration will be provided for each site as they are developed.

Existing infrastructure in Valley View Lane, located to the east, was designed to accommodate light industrial development. On-site detention will be used to offset the increases in flow associated with the planned heavy industrial development to maintain existing peak discharges. Detention is proposed for the future mixed-use development (industrial and commercial) located on the western half of the site. It is anticipated that detention will be phased as individual sites are developed. This report provides approximate detention volumes for maintaining pre-project flow rates as runoff leaves the development.

Existing 100-year floodplain inundation limits were established for Big Bear Creek Tributary, Channel BD-1 and Estelle Creek Tributary. The City of Irving has not conducted a Development Study of Estelle Creek and has no drainage study for Estelle Creek. Future development within the established Passport Park floodplains will require detailed hydraulic analysis to compare existing and proposed conditions. These streams have also been identified as Jurisdictional Features of the US and will require permitting through the USACE construction activities resulting in fill. However, an environmental assessment and permitting through Section 404 of the Clean Water Act was not a part of this drainage master plan. A separate report and study was prepared by DFW Environmental Affairs Department.

Reclamation of Bear Creek floodplain may be required for commercial sites located adjacent to International Parkway. Modifications including fill within the Bear Creek will require permitting through FEMA and the City of Irving. Permitting will also be required from DFW. Typically, hydraulic analysis is necessary to prove proposed fill will not negatively impact (increase flood level and velocities) adjacent properties. FEMA requires a Conditional Letter of Map Revision (CLOMR) prior to construction if proposed floodplain modifications within a Zone AE floodplain cause any increase in Base Flood Elevations (BFE).



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1.0 INTRODUCTION

1.1 Authorization

Pacheco Koch was retained by F.A. Peinado, LLC. on behalf of Bandera Ventures to prepare a site development drainage master plan associated with Passport Park which is an industrial development within the DFW Airport. The project is located northeast of the intersection of International Parkway and State Highway 183 in the City of Irving, Texas. This report documents the procedures and findings of the drainage analysis. Technical supporting documentation is provided in the accompanying Appendices.

1.2 Purpose

The purpose of this analysis is to develop a drainage master plan for the proposed Passport Park industrial development. This master plan defines detention requirements for the proposed development area. The detention requirements were developed by comparing pre- and post-project conditions for the 1-year, 25-year and 100-year storm events as outlined in the ISWM Criteria Manual, 2015. Existing 100-year floodplain inundation limits for three minor tributaries within the proposed development were defined. It is anticipated that a detailed floodplain reclamation plan and detailed detention configuration will be provided for each site as they are developed.

1.3 Background

Passport Park is located along the Dallas-Tarrant County line with portions of the site located in each county. Bear Creek is located to the southwest and Estelle Creek is located to the east of Passport Park. Both streams are designated as Zone AE floodplains with floodways. The Bear Creek and Estelle Creek floodplains in Dallas County are defined by the Flood Insurance Study (FIS) and the effective Flood Insurance Rate Map (FIRM) Number 48113C0285K, dated July 7, 2014. Portions of Bear Creek located to the west are within Tarrant County and are defined by the effective Flood Insurance Rate Map (FIRM) Number 48439C0235K, dated September 25, 2009. Bear Creek floodplain (100-year) within the Tarrant County portion of the site overtops International Parkway and inundates the site along the roadway. The City of Irving has not conducted a Development Study of Estelle Creek and has no drainage study for Estelle Creek.

An environmental assessment and permitting through Section 404 of the Clean Water Act was not a part of this drainage master plan. A separate report and study was prepared by DFW Environmental Affairs Department.



1.4 Project Location

The project site is located south of DFW Airport, northeast of the intersection of International Parkway and State Highway 183. A drainage divide approximately bisects the site with runoff crossing Valley View Lane to the east and International Parkway to the southwest. Figure 1 shows the approximate boundaries of Passport Park and the overall drainage divides relative to floodplain of Bear Creek and Estelle Creek.

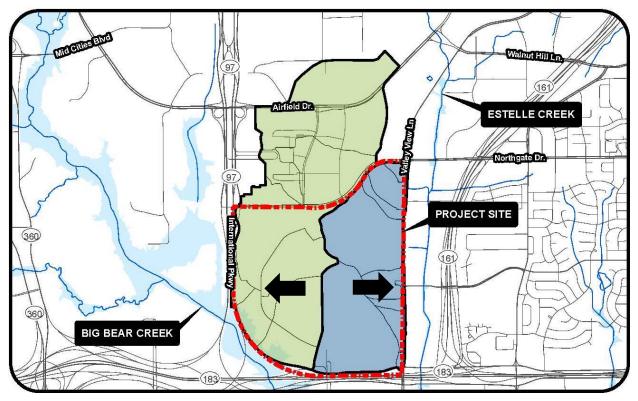


Figure 1: Location Map

1.5 Site Assessment

All storm drainage from the site leaves through culverts beneath the surrounding roadways. Eight (8) culverts cross Valley View Lane east of the site, two (2) culverts run beneath SH 183 south of the site, two (2) culverts discharge southwest of the site from under the highway interchange and two (2) culverts cross International Parkway on the west side of the site. Figure 2 shows the location of each culvert outfall.

Three (3) minor tributaries exist within the project site that are classified as Waters of the U.S. These minor tributaries do not have FEMA SFHA designation. The largest (Channel BD-1) is approximately 9550 ft long, and flows into the project site from the north and exits to the west through culvert W1 beneath International Parkway. The Big Bear Creek Tributary



is approximately 3200 ft long, and flows southwest from Mt Marvin and leaves the site on the southern edge through culvert W4 beneath the International Parkway/SH 183 interchange. The Estelle Creek Tributary is approximately 2400 ft long and exits the site through culvert E4 under Valley View Lane. Figure 2 shows the location of these three tributaries.

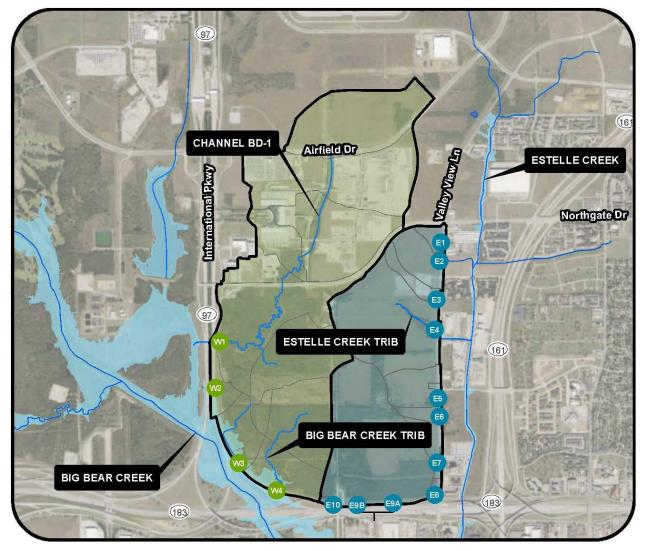


Figure 2: Culvert & Tributary Locations Map



1.6 Design Criteria

The post development design criteria is based on the NCTCOG iSWM Criteria Manual. The manual requires that all detention maintain pre-development peak discharges for 1-, 25- and 100-year 24-hour storm events. The criteria is also based on the DFW Design Criteria Manual Section 334 – Storm Drainage Utilities.

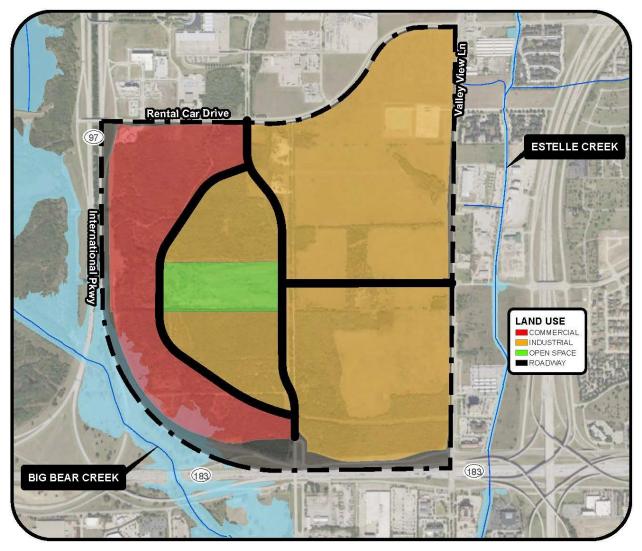


Figure 3: Proposed Improvements

1.7 Proposed Improvements

Passport Park will include a mix of industrial and commercial development. The first phase of the project includes developing plans for supporting infrastructure such as roadways and utilities as well as land development for two (2) industrial sites with multiple buildings. Figure 3 shows the proposed improvements outlined in this master plan.



2.0 SURVEY AND MAPPING

2.1 Field Survey Data

Pacheco Koch conducted an on-the-ground survey in March 2016. The survey data was then used to generate topographic information for design of the Passport Park infrastructure. Table 1 contains survey benchmarks.

BM ID	ELEVATION	DESCRIPTION
BM#1254	540.941'	BRASS DISK FOUND IN THE WEST NOSE OF A MEDIAN INTERSECTION OF RENTAL CAR DRIVE AND SOUTH 26^{TH} AVENUE ±1.1 FEET FROM BACK EDGE OF CONCRETE. POINT ALSO BEING ±26.1 FEET SOUTHEAST OF A STORM DRAINAGE MANHOLE AND 70 FEET EAST OF A LIGHT STANDARD.
BM#1255	535.562'	BRASS DISK FOUND IN THE EAST NOSE OF A MEDIAN INTERSECTION OF RENTAL CAR DRIVE AND PASSPORT AVENUE. POINT ALSO BEING ±47 FEET NORTHWEST OF A TRAFFIC SIGNAL LIGHT POLE AND ±121 FEET WEST OF LIGHT STANDARD.
BM#1256	523.405′	BRASS DISK FOUND IN THE WEST NOSE OF MEDIAN INTERSECTION OF RENTAL CAR DRIVE AND THE ENTRANCE DRIVE INTO A SHUTTLE BUS MAINTENANCE CENTER ADDRESSED AS 2425 RENTAL CAR DRIVE. POINT ALSO BEING ±47.5 FEET NORTH THE CENTER OF A CURB INLET LID AND ±74.9 FEET WEST OF A LIGHT STANDARD ON THE MEDIAN TO THE EAST.
BM#1257	527.728'	BRASS DISK FOUND IN THE NORTHEAST CORNER OF A 6-FOOT CURB INLET ON THE NORTH SIDE OF RENTAL CAR DRIVE ± 280 FEET WEST OF THE CENTERLINE OF SOUTH 24^{TH} AVENUE. POINT ALSO BEING ± 39 FEET EAST OF A LIGHT STANDARD AND 11.5 FEET WEST OF A FIRE HYDRANT.
BM#8	493.356′	BOX WITH AN "X" CUT SET ON THE NORTH SIDE OF A CONCRETE BASE OF A LIGHT STANDARD ON THE EAST SIDE OF INTERNATIONAL PARKWAY ± 1750 FEET SOUTH OF RENTAL CAR DRIVE.

Table 1: Survey Benchmarks

2.2 Project Datum

Horizontal control for the site survey data and mapping is based on the 1983 North American Datum (NAD83), Texas State Plane, North Central Zone, FIPS 4202. Vertical control is based on the 1988 North American Vertical Datum (NAVD88).

2.3 Mapping

LiDAR point cloud data and aerial photography were used to supplement the site survey data and development of watershed topography. The LiDAR data was obtained through the Texas Natural Resources Information System¹ (TNRIS) for Tarrant County (2009) and aerial photography (2010) was obtained through ArcGIS online.

¹ TNRIS: <u>http://www.tnris.org</u>



3.0 HYDROLOGY

3.1 Methodology

Hydrology for the site was reviewed using two (2) different methodologies (Rational Method for drainage to the east and Synthetic Unit Hydrographs for drainage to the southwest). In order to maintain consistency with existing plans, Rational Method was used for the east half of the site. On-site detention is anticipated to be provided for the eastern half of Passport Park as industrial sites are developed. Hydrology for the west side of the development was analyzed in this study using the computer program HEC-HMS², Hydrologic Modeling System, developed by the Hydrologic Engineering Center of the USACE (Version 4.1). Hydrology along the west side of the development compares preproject to post-project conditions to define future detention volumes needed as pad sites are developed within Passport Park.

3.2 East (Rational Method)

The individual drainage areas for the east half of the site were analyzed using Rational Method. Both pre- and post-project conditions were examined for the 1-, 25- and 100year storm events. The expected increase in peak discharges will be addressed separately with on-site detention using the Modified Ration Method for volume attenuation calculations. It is anticipated that each site will detain to the pre-project peak discharges determined for each outfall as defined in this report.

² HEC-HMS, USACE: <u>http://www.hec.usace.army.mil/software/hec-hms/</u>



Drainage Area

Drainage areas of available as-built plans of adjacent roads surrounding the project site (see Appendix A) were reviewed in conjunction with topographic data to establish preproject drainage areas divides for the eastern half of the site. Outfall drainage areas were developed by combining relevant sub-basins identified in the as-built plans. Figure 4 shows the drainage area delineation of the eastern side of Passport Park.

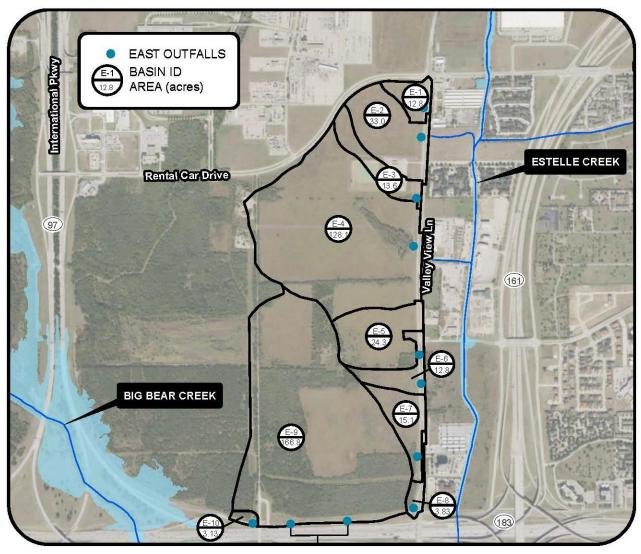


Figure 4: Eastern Drainage Delineation



Design Storm Intensities

Design storm intensities were determined from the NCTCOG, ISWM Technical Manual, 2015³. Times of concentration were calculated for each individual sub-basin to calculate the design storm intensity for each respective basin. Times of concentration for post-development conditions were assumed to be 10 minutes (minimum). Calculations for the times of concentration are provided in Appendix A.

<u>C-Factors</u>

An area-weighted average of C-factors for existing conditions was determined for each outfall location based on combined sub-basins identified in the as-built plans. Figure 5 shows the existing C-factors used to compute the weighted C-factor for each basin.

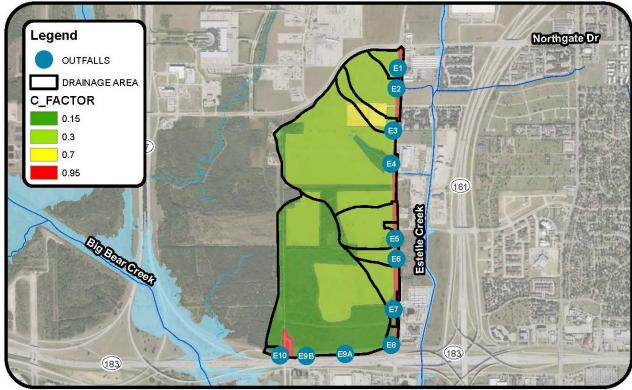


Figure 5: C Factor Map

³ NCTCOG, ISWM Technical Manual: <u>http://iswm.nctcog.org/Documents/technical_manual/Hydrology_9-2014.pdf</u>



3.3 West (Synthetic Unit Hydrograph Method)

As-built plans for the International Parkway were limited and information related to culvert capacity was not verifiable. New hydrology was developed and pre-project peak discharges and approximate detention volumes for the western half of Passport Park were established based on the SCS Curve Number Method. It is anticipated that detention will be provided during future phases of development as pad sites are constructed. Additional detention volumes will be required throughout the developed drainage areas to reduce peak discharges to back to pre-project conditions. This study does not define the location of required detention areas within each drainage sub-basin.

Drainage Area

Drainage areas of available as-built plans of adjacent roads surrounding the project site (see Appendix A) were reviewed in conjunction with topographic data to establish preproject drainage areas divides for the western half of the site. Approximately 420 acres of off-site drainage is conveyed through the site to Bear Creek. Figure 6 shows the drainage area delineation of the western side of Passport Park.

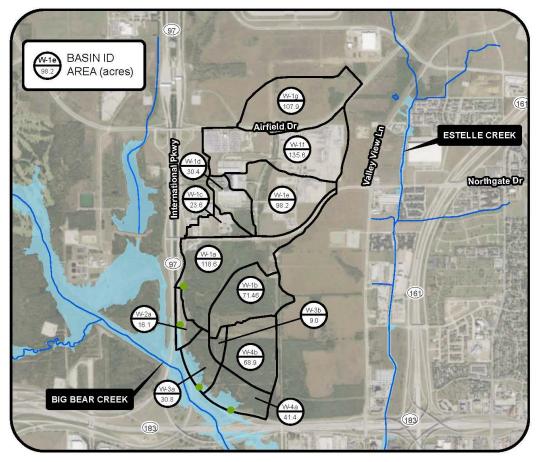


Figure 6: Western Drainage Delineation



<u>Synthetic Storm</u>

The hydrologic model is based 24-hour duration storm event using the SCS Type III Rainfall Distribution Method. The depths used to develop the rainfall distribution were obtained from the iSWM Technical Manual Tarrant County Rainfall Data. Table 2 shows the 1-, 25- and 100-year rainfall depths used in the rainfall distribution.

Duration	1-Year	25-Year	100-Year
	Depth (in)	Depth (in)	Depth (in)
24 hours	2.64	6.72	9.12

Table 2: Frequency Storm Depths

Loss Rates

Loss rates and initial abstractions were determined from the Curve Number method outlined in US Department of Agriculture, Technical Release No. 55, Urban Hydrology for Small Watersheds⁴. Composite Curve Numbers for the sub-basin containing the proposed development were updated based on the hydrologic soil types and the existing land use for the City of Irving. The study area consists primarily of hydrologic soil type D, with a few isolated areas of types B. Hydrologic soil types were determined from the USDA-NRCS Soil Survey Geographic.⁵ (SSURGO) database for Dallas and Tarrant Counties, Texas dated 2009. Curve Numbers were used in calculating existing and proposed peak discharges. Land Use and Soil Maps along with Curve Number computations are provided in Appendix A.

Lag Time

Times of Concentration were determined for each sub-basin from the method outlined in Chapter 3 of Technical Release No. 55. Overland flow distances were limited to 100feet. The shallow concentrated flow components use a K-factor of 16.1 and 20.3 for unpaved and paved conditions, respectively. Times of Concentration for the project site under post-project conditions were assumed to be the minimum (10 min) as defined by iSWM. Basin lag times were developed by multiplying the time of concentration by 0.6. Lag Time calculations are provided in Appendix A.

Unit Hydrographs and Routing

The Soil Conservation Service Dimensionless Unit Hydrograph Method was used to produce a synthetic hydrograph for the given 24-hour storms. The hydrograph parameters used for each sub-basin were based on the sub-basin Lag Time and the composite Curve Numbers (discussed above). Hydrographs from each sub-basin were routed to combination points using the Muskingum-Cunge. Level Pool Routing was used to determined proposed detention volumes. A computational interval of 2 minutes was used in HEC-HMS to develop hydrographs for each sub-basin.

⁵ USDA-NRCS: <u>http://soildatamart.nrcs.usda.gov</u>



⁴ TR-55, NRCS: <u>http://www.wsi.nrcs.usda.gov/products/w2q/H&H/docs/other/TR55_documentation.pdf</u>

4.0 HYDRAULICS

4.1 Methodology

Three separate streams (Big Bear Creek Tributary, Channel BD-1and Estelle Creek Tributary) located in Passport Park were analyzed using the computer program HEC-RAS⁶, River Analysis System, developed by the Hydrologic Engineering Center of the USACE (Version 5.0.3, October 2016). The existing conditions hydrology determined in the Passport Park Drainage Master plan was used to establish 100-year (1% annual chance) peak discharges for each model. The hydraulic model includes all three streams. Separate geometry and plans were developed for each stream. The procedures used in developing the hydraulic models are further explained below.

4.2 Existing Conditions (ECM)

The existing Conditions models for Big Bear Creek Tributary, Channel BD-1 and Estelle Creek Tributary were developed to map existing inundation limits for the 100-year floodplain. Supporting data, results and mapping for each of the three (3) streams are provided in Appendix C.

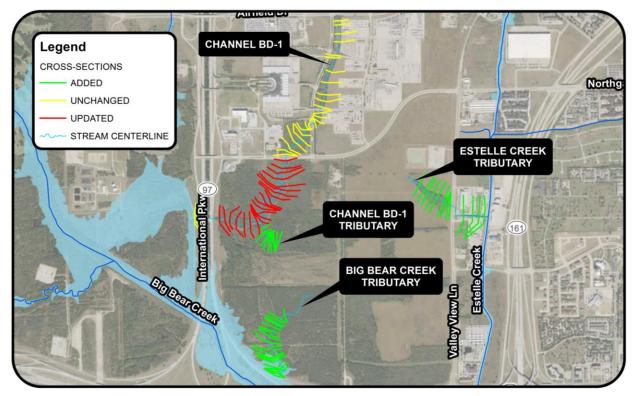


Figure 7: Cross-Section Layout

⁶ HEC-RAS, USACE: <u>http://www.hec.usace.army.mil/software/hec-ras/</u>



Channel BD-1

DFW Airport provided the existing conditions hydraulic model for Channel BD-1, prepared by Jacob's, dated 2014. The existing model contains 48 cross-sections. Cross sectional geometry was updated for the 22 sections located within Passport Park. The model was revised to include 11 sections for a minor tributary located upstream of Section 2032 of the main reach. The downstream boundary condition was unrevised from the original model. Roughness coefficients for cross-sections within Passport Park were range from 0.075 for the channel and 0.12 for the heavily wooded overbanks. These values were unrevised from the original model. Normal contraction and expansion coefficients were used for all sections of 0.1 and 0.3, respectively.

Big Bear Creek Tributary

An existing hydraulic model for Big Bear Creek Tributary was not available. A new model was created for existing conditions extending northward from West Airport Freeway approximately 2,000 linear-feet. The geometry for the hydraulic model was developed by adding 22 new cross-sections from the site survey data within Passport Park. A normal depth slope of 0.001 was used for the starting boundary condition. Roughness coefficients for this tributary range from were range from 0.075 for the channel and 0.12 for the heavily wooded overbanks. Normal contraction and expansion coefficients of 0.1 and 0.3, were used for all cross sections, respectively.

Estelle Creek Tributary

An existing hydraulic model for Estelle Creek Tributary was not available. A new model was created for existing conditions extending westward from Estelle Creek and Valley View Lane, approximately 2,000 linear-feet. The geometry for the hydraulic model was developed by adding 13 new cross-sections and the Valley View Lane culvert. from the site survey data within Passport Park and as-built plans. A known water-surface elevation (499.1) was used for the starting boundary conditions of the hydraulic model. The known WSEL is based on Estelle Creek Base Flood Elevation as defined by FEMA's FIS for Dallas, County Texas Volume 4 of 9. Roughness coefficients for this tributary range from 0.018 for the downstream concrete channel to 0.075 for the moderately wooded overbanks. Contraction/expansion coefficients were set to 0.3 and 0.5 for cross-sections located up and downstream of the culvert sections, respectively. Normal contraction and expansion coefficients of 0.1 and 0.3, were used for all remaining cross sections.



5.0 RESULTS

5.1 Hydrologic Results

This master drainage plan provides peak discharges for the eastern and western portions of Passport Park. On-site detention will be provided on a site by site basis for the eastern half of the development. The western half also includes proposed detention volumes required to maintain pre-project peak discharges.

East Results

Figure 8 and Table 4 show the outfall locations and peak discharges for pre- and postproject conditions, respectively. Culverts 9A and 9B have a common outfall for the given drainage area. It is anticipated that the total flow will be divided and distributed equally to each inlet.

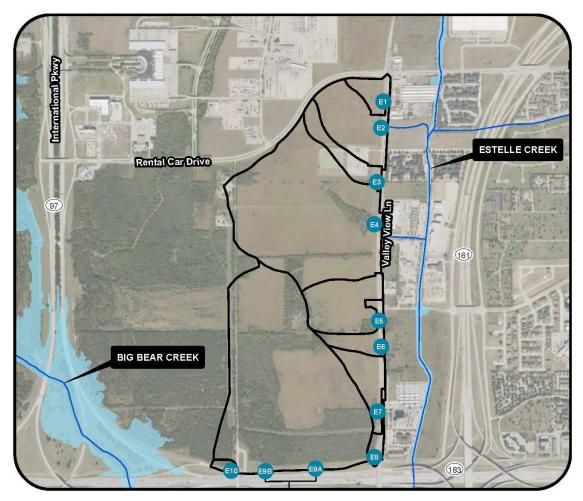


Figure 8: Eastern Drainage Area Outfall Locations



Table 3 shows the calculated Rational Method pre-project and post-project peak discharges for the 100-year storm event. On-site detention for each industrial site is required to maintain pre-project peak discharges.

Culvert/Drainage Area	100-Year Pre-Project Peak Discharge (Cfs)	100-Year Post-Project Peak Discharge (Cfs)
E1	24.9	77.2
E2	73.5	274.2
E3	38.0	121.8
E4	242.9	1188.2
E5	74.5	261.9
E6	39.9	103.5
E7	51.7	144.4
E8	23.6	39.9
E9A/E9B	244.2	1547.1*
E10	9.2	18.9
Tuble 1	Dentional Made ad Dould	Dia a la sussa a

 Table 3: Rational Method Peak Discharges

* The 100-year post-project peak for Drainage Areas E9A and E9B is the undetained release rate. Based on input from the City of Irving, the downstream channel on the south side of SH 183 does not have capacity for the undetained release rate. Development within subbasins E9A and E9B will be required to detain the 100-year post-project peak discharges to the pre-project peak discharge shown in the table above. It should be noted, the design plans for the Gateway Business Park Passport South Industrial development show the100-year post-project peak discharge is approximately 227.6 cfs, which is 16.6 cfs below the pre-project conditions.



West Results

Figure 9 show the outfall locations and potential detention footprints for the western half of the development. Detention footprint areas were approximated based establishing a volume to maintaining pre-project peak discharges for the 1-, 25- and 100-year storm events as required in the iSWM Manual. Detailed calculations will be required as specific sites are developed during later phases of the project. The location and size of detention footprints shown in Figure 9 are for site planning purposes only. Detailed detention calculations and grading plans will be required for each site.

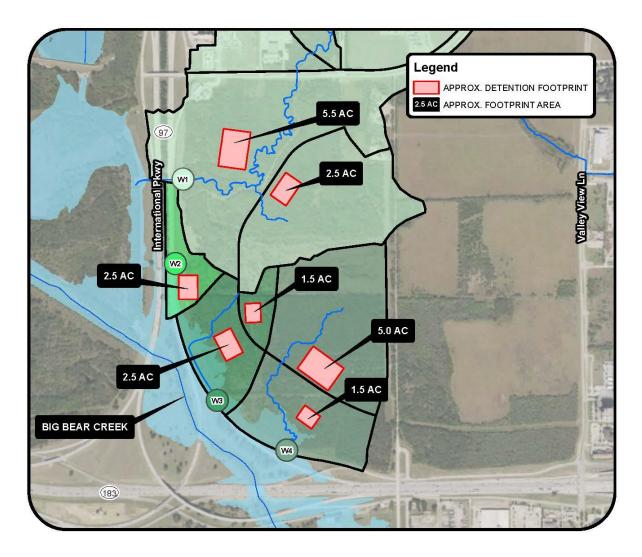


Figure 9: Western Drainage Area Outfall Locations



Figure 10 shows the overall watershed for the western half of Passport Park. The area located between Rental Car Drive and Airfield Drive was assumed to be developed. The area north of Airfield Drive is currently undeveloped and may need to provide detention.

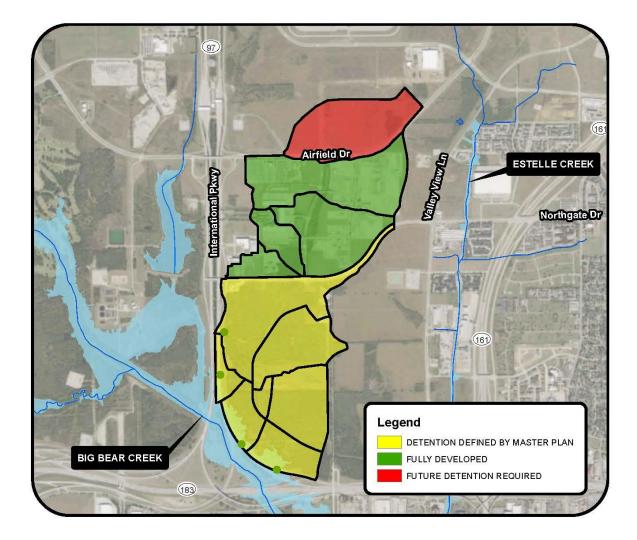


Figure 10: Future Detention Requirements



Table 4 shows the 100-year peak discharges for pre- and post-project conditions for each sub-basin on the west half of the site. Peak discharges for sub-basins upstream of the site are unchanged. On-site, peak discharges increase from pre- to post-project conditions, as expected.

Sub- basin	100-Yr Pre-Project Peak Discharge (cfs)	100-Yr Post-Project Peak Discharge (cfs)
W-1a	507	868
W-1b	331	511
W-1c	125	125
W-1d	180	180
W-le	515	515
W-1f	603	603
W-1g	481	481
W-2a	74	118
W-3a	118	223
W-3b	56	64
W-4a	157	301
W-4b	318	490

 Table 4: 100-Year Peak Discharge Comparison

Table 5 shows the computed pre-project discharge rates at each outfall location. Postproject rates must not exceed the values indicated in Table 5. The table also provides the total estimated detention volume necessary to reduce developed peak discharges to pre-project peak discharges.

	1-Yr Pre-Project	25-Yr Pre-Project	100-Yr Pre-Project	Required
Culvert	Peak Discharge	Peak Discharge	Peak Discharge	volume
	(cfs)	(cfs)	(cfs)	(ac-ft)
W1	502	1750	2500	32.0
W2	8	50	74	5.0
W3	16	113	180	9.0
W4	58	310	474	20.0

Table 5: Detention Requirements



5.2 Hydraulic Results

Figure 11 shows the existing 100-year floodplain inundation limits for the three streams within Passport Park. Detailed floodplain mapping and water-surface elevations are provided in Appendix B. Hydraulic model output is provided in Appendix C.

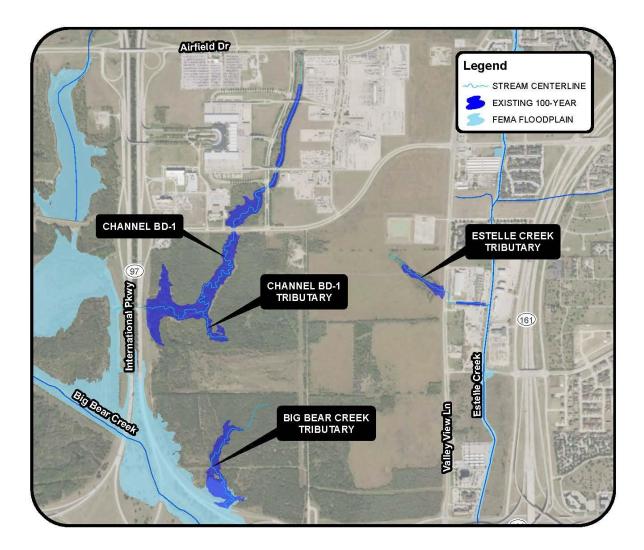


Figure 11: Existing Conditions Floodplain



6.0 CONCLUSION & RECOMMENDATIONS

This study develops a master drainage plan for the proposed Passport Park industrial development. Pre-project peak discharges are established for the eastern side of the development based on as-built plans of existing downstream storm water infrastructure using Rational Method calculations. On-site detention will be required to reduce developed flows and maintain pre-project peak discharges for individual industrial sites. The western half of the development was analyzed using a 24-hour frequency storm and the unit hydrograph methodology. Pre-project peak discharges for the 1-, 25-, and 100-year storm events were established base on pre-project watershed conditions. Estimated detention volumes and footprint areas are provided for Passport Park planning purposes. Detailed detention calculations will be required as development occurs. This study does not define the location of required detention areas within each drainage sub-basin.

Existing 100-year floodplain inundation limits were established for Big Bear Creek Tributary, Channel BD-1 and Estelle Creek Tributary. These minor tributaries are not currently shown on the FEMA Flood Insurance Rate Maps. However, future development including modifications to the established floodplains within Passport Park will require detailed hydraulic analysis to compare existing and proposed conditions. These streams have also been identified as Jurisdictional Features of the US and will require permitting through the USACE construction activities resulting in fill.

Reclamation of Bear Creek floodplain may be required for commercial sites located adjacent to International Parkway. Modifications including fill within the Bear Creek will require permitting through FEMA and the City of Irving. Permitting will also be required from DFW. Typically, hydraulic analysis is necessary to prove proposed fill will not negatively impact (increase flood level and velocities) adjacent properties. FEMA requires a Conditional Letter of Map Revision (CLOMR) prior to construction if proposed floodplain modifications within a Zone AE floodplain cause any increase in Base Flood Elevations (BFE).



7.0 DEFINITIONS & ACRONYMS

<u>100-Year Flood</u>. The flood event that has a 1-percent chance of being equaled or exceeded each year, also referred to as the 1-percent annual chance flood.

<u>Base Flood Elevation (BFE)</u>. Typically refers to the water-surface elevations during the 100year flood event.

<u>Basin Lag Time</u>. The time difference between the peak of the storm event and the peak discharge. Typically calculated by multiplying the time of concentration by 0.6.

<u>Curve Number (CN)</u>. A hydrologic parameter used to characterize the runoff properties for a particular soil type and land use.

FPS. Feet Per Second

<u>HEC-HMS</u>. The Hydrologic Engineering Center – Hydrologic Modeling System software developed by the US Army Corps of Engineers to simulate the precipitation-runoff processes of dendritic watershed systems.

NAD83. 1983 North American Datum

NAVD88. 1988 North American Vertical Datum

<u>PK</u>. Pacheco Koch

<u>Time of Concentration (Tc)</u>. The time needed for water to flow from the most hydraulically remote point in a watershed to the watershed outlet. It is a function of the topography, geology, and land use within the watershed.

<u>USACE</u>. United States Army Corps of Engineers

<u>WSEL</u>. Water-Surface Elevation



8.0 **REFERENCES**

Department of Agriculture. Natural Resources Conservation Service. Technical Release 55, Urban Hydrology for Small Watersheds. Washington, DC: GPO, 1986.

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Ernest F. Brater, Horace Williams King: Handbook of Hydraulics, Sixth Edition, Michigan, 1976.

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United States Army Corps of Engineers. Hydrologic Engineering Center: HEC-HMS Hydrologic Modeling System: [Computer Software, User's Manual, Technical Reference Manual, Application Guide], Version 4.1. Washington, DC: GPO, August 2010.

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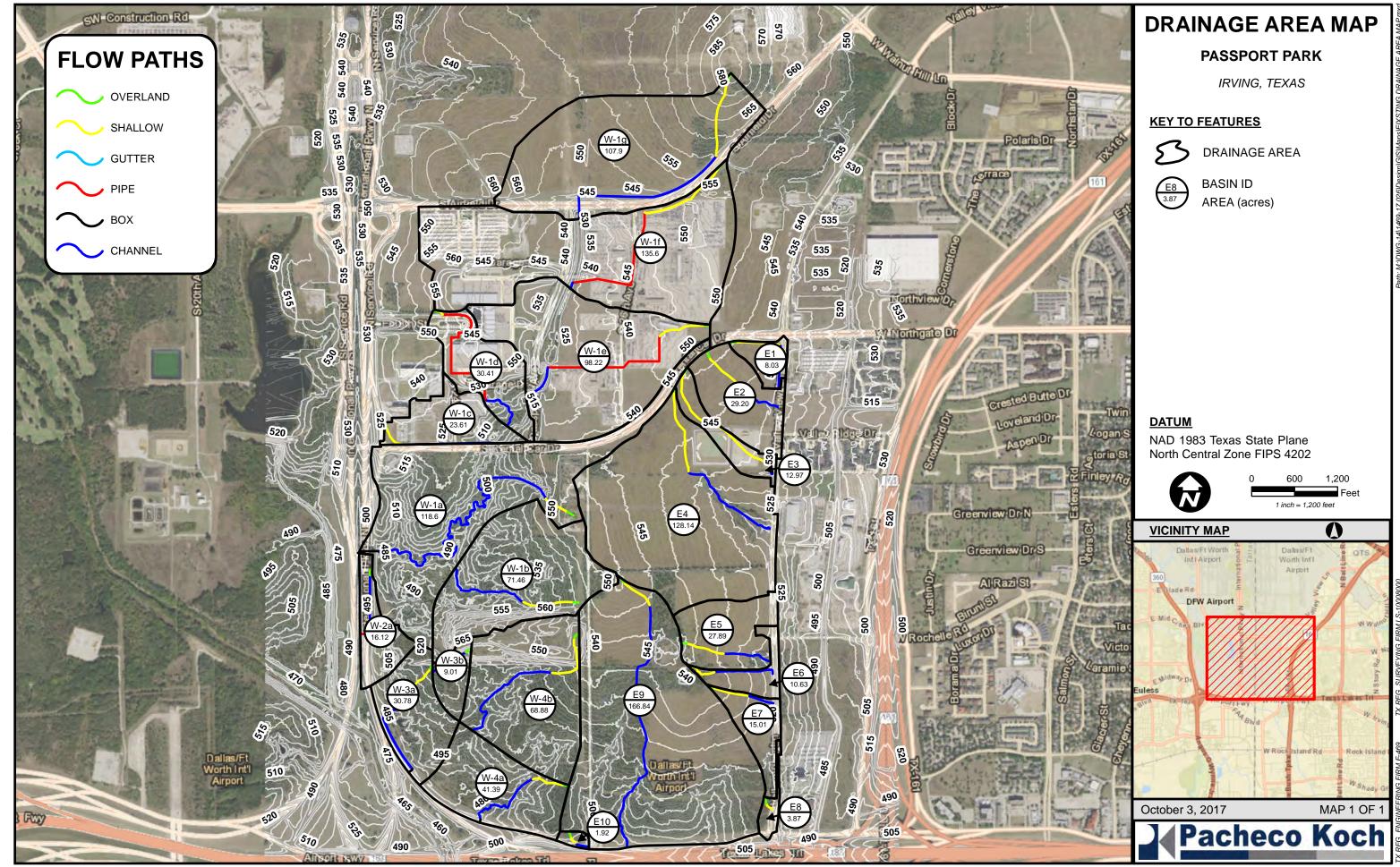


Appendix A

Hydrology

- Drainage Area Map
- Hydrologic Soil Groups Map
- Existing Land Use Map
- Proposed Land Use Map
- Existing C Factor Map
- Proposed C Factor Map
- Curve Number Calculations
- Lag Time Calculations
- SCS Hydrologic Parameters
- Weighted C Factor
 Calculations

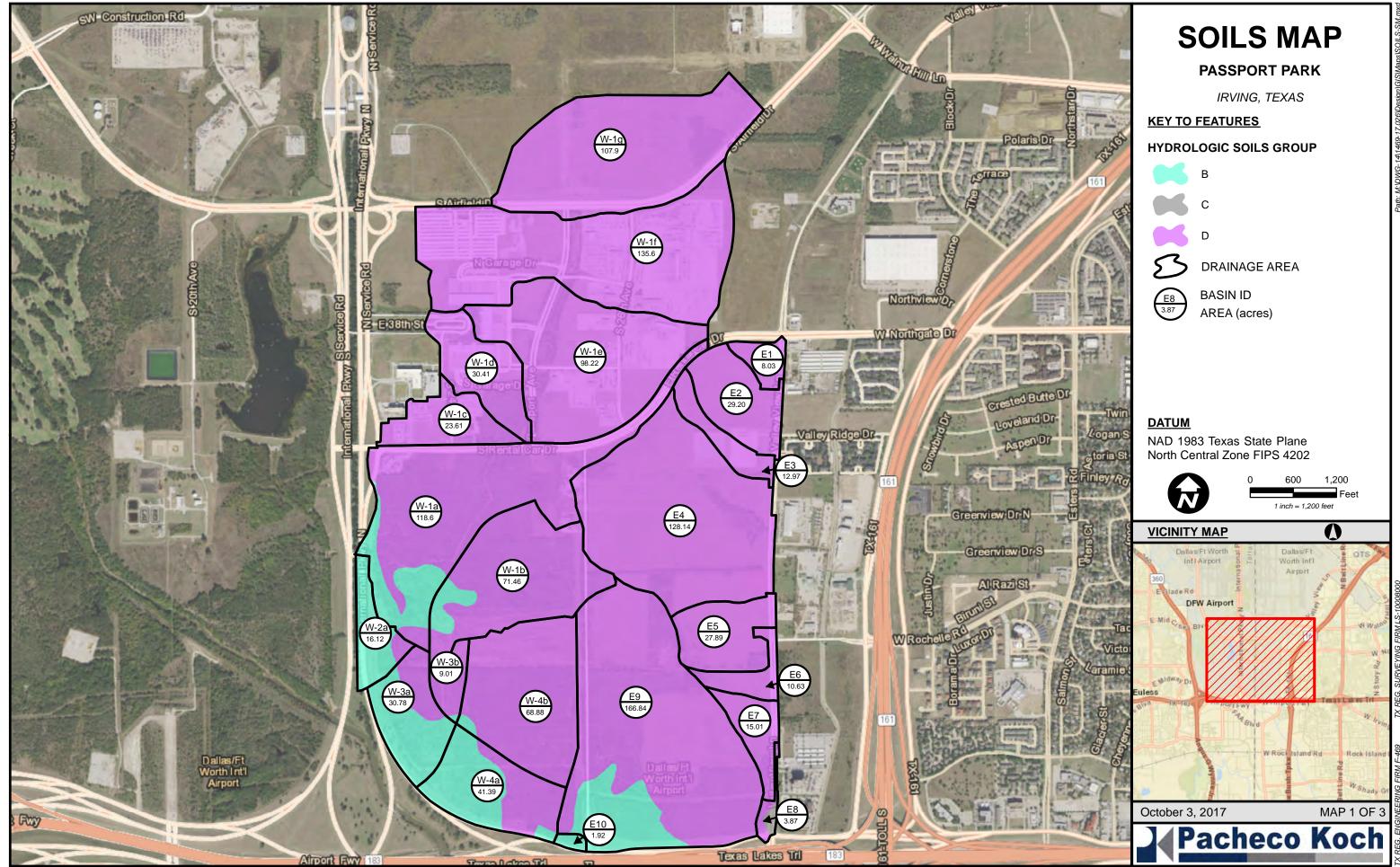
Drainage Area Map





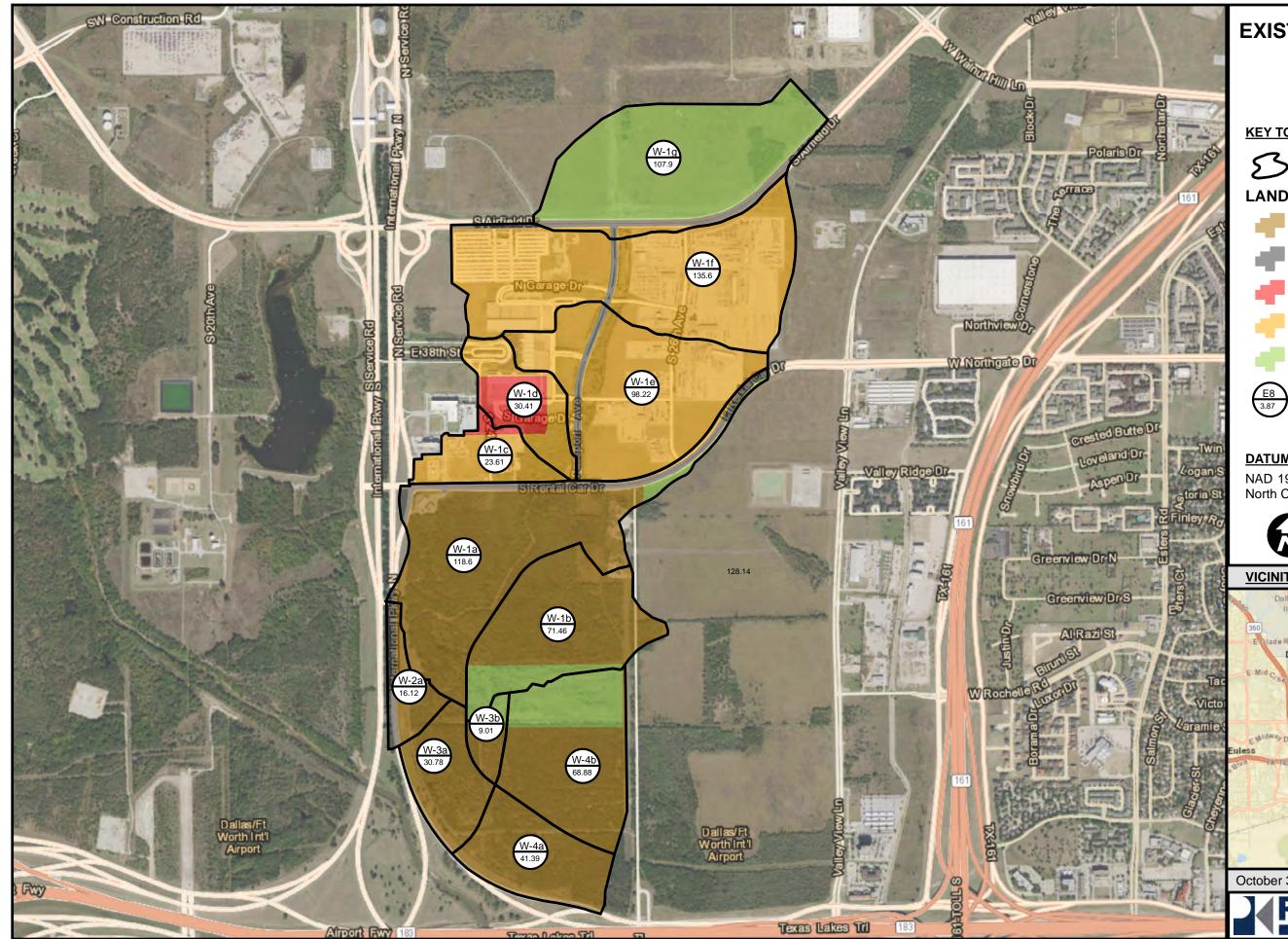


Hydrologic Soil Groups Map



B	
E8	

Existing Land Use Map

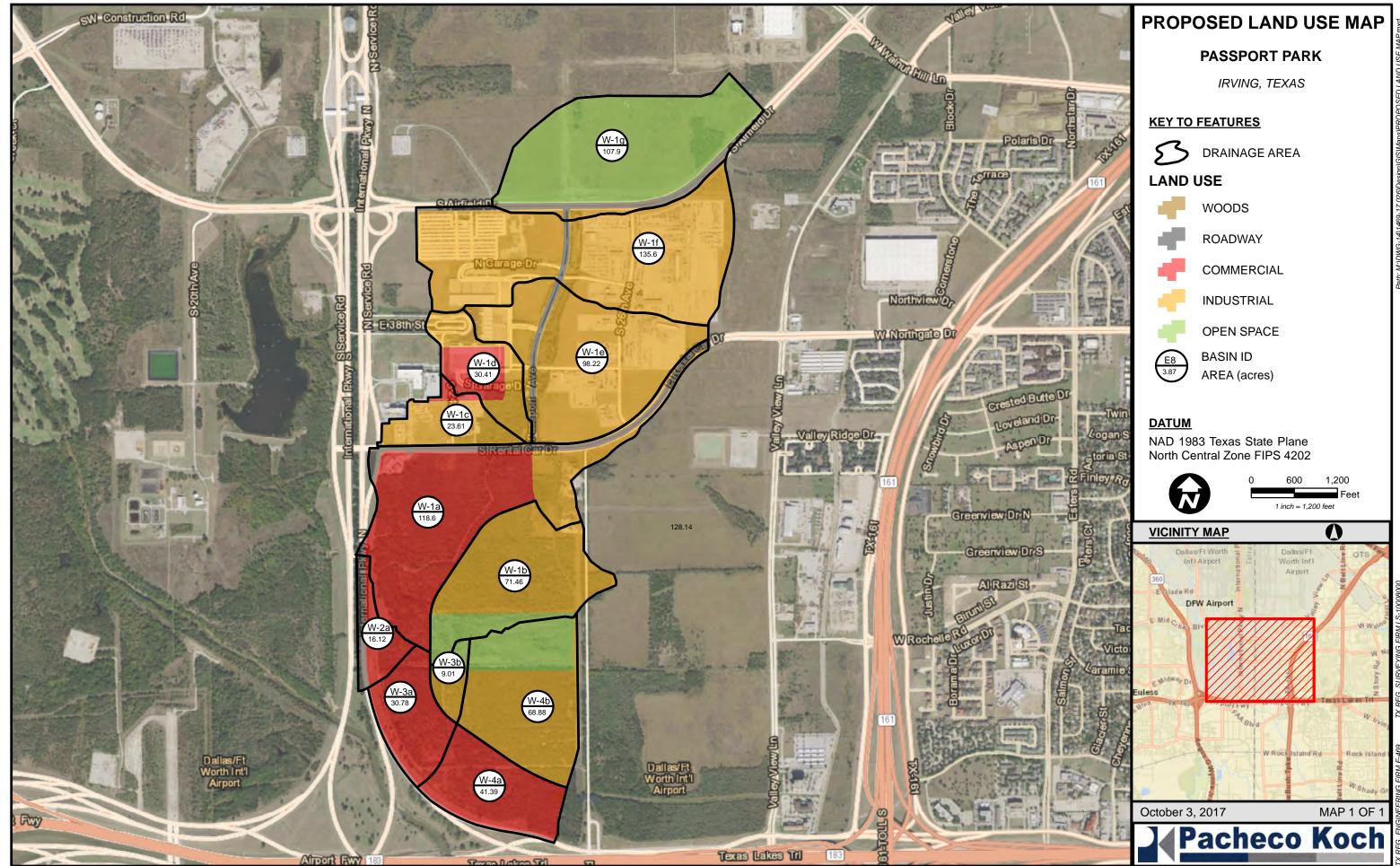


EXISTING LANDUSE MAP PASSPORT PARK

IRVING, TEXAS

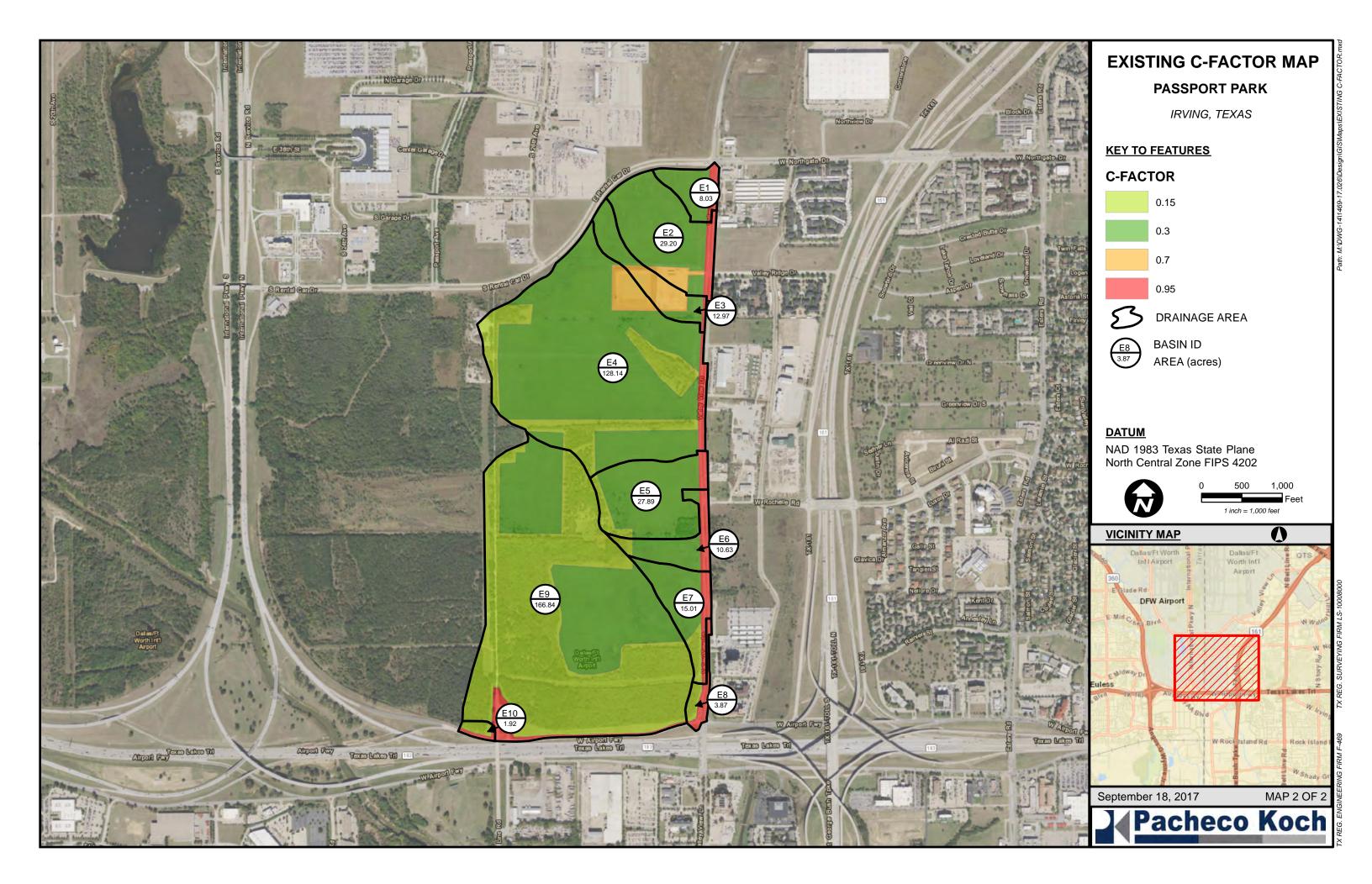
<u>КЕҮ ТО</u>	FEATURES	ign\Gl
B	DRAINAGE AREA	Path: M:\DWG-14\1469-17.026\Design\GIS\
LAND	USE	4/1469-17
	WOODS	-1-9MG
- 4E	ROADWAY	Path: M.
	COMMERCIAL	
	INDUSTRIAL	
	OPEN SPACE	
E8 3.87	BASIN ID AREA (acres)	
	33 Texas State Plane Intral Zone FIPS 4202	
	0 600 1,200 Feet 1 inch = 1,200 feet	
	VFt Worth 🚆 🗐 Dallas/Ft 🧯 oTS	
360 E Glade Rd	Airport Worth Int'l Airport Airport W Airport W	10008000
E Mid Cries		16 FIRM LS-10008000
Euless	S Py Kot SN	
E thidway Dr.	W Rock Island Rd	TX REG. SURVEYING
E thidway Dr.	3 PU ASINE N 3 PU ASINE N 4 Frank State 4 Frank State 5 Frank	TX REG. SURVEYING
Euless Bird Tax-Tas October 3,	Port wy Port wy Por	

Proposed Land Use Map

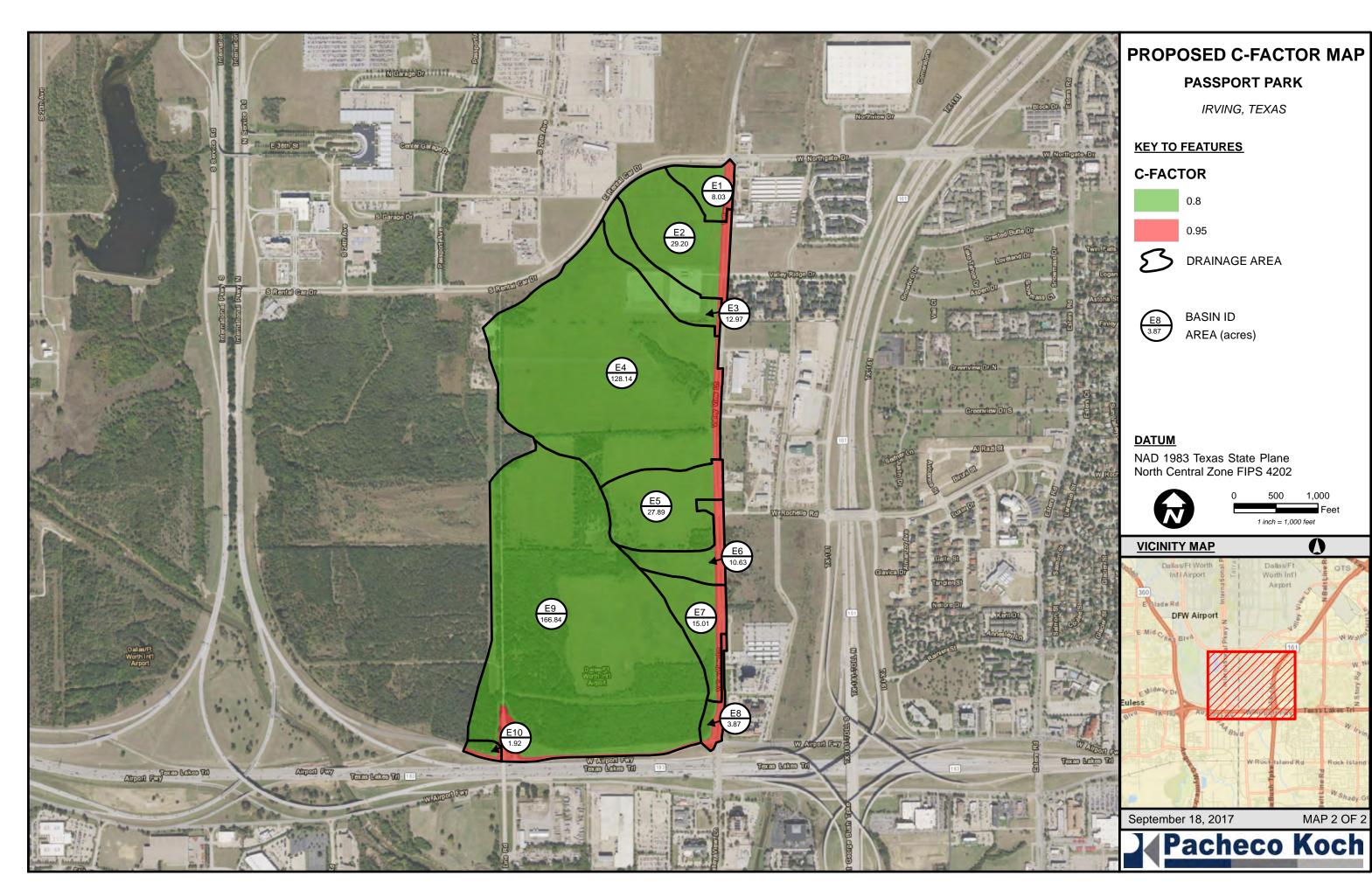


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Existing C Factor Map



Proposed C Factor Map



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9 TX REG. SURVEYING FIRM LS-10

Curve Number Calculations

PRE-PROJECT CURVE NUMBER REPORT

W-1a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
INDUSTRIAL	D	93	117,040	2.1
OPEN SPACE (FAIR CONDITION)	В	69	11	0.0
OPEN SPACE (FAIR CONDITION)	D	84	139,669	2.3
ROADWAY	В	98	18,758	0.4
ROADWAY	D	98	473,308	9.0
WOODS	В	60	771,517	9.0
WOODS	D	79	3,646,439	55.8
			5,166,742	78.4

W-1b

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
OPEN SPACE (FAIR CONDITION)	В	69	83,324	1.8
OPEN SPACE (FAIR CONDITION)	D	84	469,922	12.7
WOODS	В	60	164,142	3.2
WOODS	D	79	2,395,561	60.8
			3,112,950	78.5

W-1c

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
COMMERCIAL & BUSINESS	D	95	99,342	9.2
INDUSTRIAL	D	93	925,686	83.7
ROADWAY	D	98	3,557	0.3
			1,028,585	93.2

W-1d

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
COMMERCIAL & BUSINESS	D	95	573,955	41.2
INDUSTRIAL	D	93	742,308	52.1
ROADWAY	D	98	8,472	0.6
			1,324,735	93.9

W-1e

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
INDUSTRIAL	D	93	4,097,721	89.1
ROADWAY	D	98	180,527	4.1
			4,278,249	93.2

W-1f

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
INDUSTRIAL	D	93	5,770,046	90.8
ROADWAY	D	98	137,033	2.3
			5,907,079	93.1

W-1g

land use	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
INDUSTRIAL	D	93	147,896	2.9
OPEN SPACE (FAIR CONDITION)	D	84	4,180,872	74.7
ROADWAY	D	98	370,277	7.7
			4,699,045	85.4

W-2a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
ROADWAY	В	98	223,370	31.2
WOODS	В	60	401,710	34.3
WOODS	D	79	77,164	8.7
			702,244	74.2

W-3a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
OPEN SPACE (FAIR CONDITION)	D	84	26	0.0
ROADWAY	В	98	36,416	2.7
WOODS	В	60	923,577	41.3
WOODS	D	79	380,828	22.4
			1,340,847	66.4

W-3b

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
OPEN SPACE (FAIR CONDITION)	D	84	125,397	26.8
WOODS	В	60	11,141	1.7
WOODS	D	79	256,072	51.5
			392,610	80.1

W-4a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
ROADWAY	В	98	41,992	2.3
ROADWAY	D	98	14,630	0.8
WOODS	В	60	1,031,658	34.3
WOODS	D	79	714,481	31.3
			1,802,761	68.7

W-4b

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	WEIGHTED CN
OPEN SPACE (FAIR CONDITION)	D	84	929,036	26.0
WOODS	В	60	46,276	0.9
WOODS	D	79	2,024,931	53.3
			3,000,242	80.3

W-1a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	В	92	771,343	13.7
COMMERCIAL & BUSINESS	D	95	2,996,618	55.1
INDUSTRIAL	В	88	174	0.0
INDUSTRIAL	D	93	906,483	16.3
OPEN SPACE (FAIR CONDITION)	В	69	11	0.0
OPEN SPACE (FAIR CONDITION)	D	84	48	0.0
ROADWAY	В	98	1,565	0.0
ROADWAY	В	98	17,192	0.3
ROADWAY	D	98	473,308	9.0
			5,166,742	94.5

W-1b

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	В	92	61	0.0
COMMERCIAL & BUSINESS	D	95	291	0.0
INDUSTRIAL	В	88	164,081	4.6
INDUSTRIAL	D	93	2,395,271	71.6
OPEN SPACE (FAIR CONDITION)	В	69	83,324	1.8
OPEN SPACE (FAIR CONDITION)	D	84	469,922	12.7
			3,112,950	90.7

W-1c

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	D	95	99,342	9.2
INDUSTRIAL	D	93	925,686	83.7
ROADWAY	D	98	3,557	0.3
			1,028,585	93.2

W-1d

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	D	95	573,955	41.2
INDUSTRIAL	D	93	742,308	52.1
ROADWAY	D	98	8,472	0.6
			1,324,735	93.9

W-1e

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
INDUSTRIAL	D	93	4,097,721	89.1
ROADWAY	D	98	180,527	4.1
			4,278,249	93.2

W-1f

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
INDUSTRIAL	D	93	5,770,046	90.8
ROADWAY	D	98	137,033	2.3
			5,907,079	93.1

W-1g

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
INDUSTRIAL	D	93	147,896	2.9
OPEN SPACE (FAIR CONDITION)	D	84	4,180,872	74.7
ROADWAY	D	98	370,277	7.7
			4,699,045	85.4

W-2a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	В	92	401,710	52.6
COMMERCIAL & BUSINESS	D	95	77,164	10.4
ROADWAY	В	98	223,370	31.2
			702,244	94.2

W-3a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	В	92	923,577	63.4
COMMERCIAL & BUSINESS	D	95	380,614	27.0
INDUSTRIAL	D	93	214	0.0
OPEN SPACE (FAIR CONDITION)	D	84	26	0.0
ROADWAY	В	98	36,416	2.7
			1,340,847	93.0

W-3b

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	В	92	18	0.0
COMMERCIAL & BUSINESS	D	95	115	0.0
INDUSTRIAL	В	88	11,123	2.5
INDUSTRIAL	D	93	255,957	60.6
OPEN SPACE (FAIR CONDITION)	D	84	125,397	26.8
			392,610	90.0

W-4a

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	В	92	1,031,658	52.6
COMMERCIAL & BUSINESS	D	95	714,163	37.6
INDUSTRIAL	D	93	318	0.0
ROADWAY	В	98	41,992	2.3
ROADWAY	D	98	14,630	0.8
			1,802,761	93.4

W-4b

LAND USE	SOIL TYPE	CURVE NUMBER	SHAPE AREA	AREA WEIGHTED CN
COMMERCIAL & BUSINESS	D	95	217	0.0
INDUSTRIAL	В	88	46,276	1.4
INDUSTRIAL	D	93	2,024,714	62.8
OPEN SPACE (FAIR CONDITION)	D	84	929,036	26.0
			3,000,242	90.1

Lag Time Calculations

EAST DRAINAGE TIME OF CONCENTRATION REPORT

EQUATIONS:	
$T_{\text{overland}} = \frac{0.42(n \cdot L)^{0.8}}{(P_{2YR})^{0.5} S^{0.4}}$	$T_{channel} = \frac{L}{60 \cdot K \cdot S^{0.5}}$
P-2YR = 4 INCH	MNIMUM SLOPE USED - 0.5%

E-01

FLOW TYPE	SURFACE	length (f	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps) Tc (min)
OVERLAND	GRS-DENSE	100	0.60	0.240	0.00	0.1	22.57
SHALLOW	UNPAVED	638	1.33	0.000	16.10	1.9	5.72
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	600	1.27	0.050	28.69	3.2	3.09
		1,338					31.38

E-02

FLOW TYPE	SURFACE	LENGTH (ft) SLOPE (%)		ROUGHNESS	k value	VELOCITY (fps) Tc (min)
OVERLAND	GRS-DENSE	100	0.42	0.240	0.00	0.1	25.97
SHALLOW	UNPAVED	896	0.97	0.000	16.10	1.6	9.41
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	337	2.03	0.050	28.69	4.1	1.37
		1,333					36.75

E-03

FLOW TYPE	SURFACE	length (f	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fp:	s) Tc (min)
OVERLAND	GRS-DENSE	100	0.50	0.240	0.00	0.1	24.25
SHALLOW	PAVED	975	2.57	0.000	20.30	3.3	4.99
SHALLOW	UNPAVED	924	0.60	0.000	16.10	1.2	12.38
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	171	6.56	0.050	28.69	7.3	0.39
		2,170					42.01

E-04

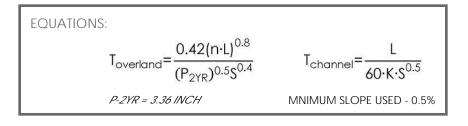
FLOW TYPE	SURFACE	LENGTH (f	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps)	Tc (min)
OVERLAND	GRS-DENSE	100	0.83	0.240	0.00	0.1	19.76
SHALLOW	UNPAVED	1,143	0.67	0.000	16.10	1.3	14.43
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	1,525	4.95	0.050	28.69	6.4	3.98
		2,768					38.17

E-05

FLOW TYPE	SURFACE	length (f	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps)) Tc (min
OVERLAND	GRS-DENSE	100	1.47	0.240	0.00	0.1	15.75
SHALLOW	UNPAVED	516	1.55	0.000	16.10	2.0	4.28
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	685	2.72	0.050	28.69	4.7	2.41
		1,301					22.45
E-06							
FLOW TYPE	SURFACE	length (f	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fps)) Tc (min
OVERLAND	GRS-DENSE	100	1.26	0.240	0.00	0.1	16.76
SHALLOW	UNPAVED	367	1.14	0.000	16.10	1.7	3.55
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	866	2.43	0.050	28.69	4.5	3.23
		1,333					23.54
E-07							
FLOW TYPE	SURFACE	length (f	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fps)) Tc (mir
OVERLAND	GRS-DENSE	100	0.44	0.240	0.00	0.1	25.62
SHALLOW	UNPAVED	527	1.34	0.000	16.10	1.9	4.71
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	351	3.06	0.050	28.69	5.0	1.17
		978					31.50
E-08							
FLOW TYPE	SURFACE	LENGTH (f	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fps)) Tc (mir
OVERLAND	GRS-DENSE	100	1.27	0.240	0.00	0.1	16.71
SHALLOW	UNPAVED	121	3.31	0.000	16.10	2.9	0.69
		221					17.39
E-09							
FLOW TYPE	SURFACE	length (f	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fps)) Tc (mir
OVERLAND	GRS-DENSE	100	0.66	0.240	0.00	0.1	21.71
SHALLOW	UNPAVED	467	1.22	0.000	16.10	1.8	4.39
CHANNEL	NATRL TRAP (B=4,Y=3,SS=3:1)	3,715	2.83	0.050	42.29	7.1	8.71
		4,282					34.81

FLOW TYPE	SURFACE	length (f	t) slope (%)	ROUGHNESS	k value	VELOCITY (fps)) Tc (min)
OVERLAND	GRS-DENSE	100	4.14	0.240	0.00	0.2	10.41
SHALLOW	UNPAVED	98	5.48	0.000	16.10	3.8	0.43
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	202	6.89	0.050	28.69	7.5	0.45
		401					11.29

TIME OF CONCENTRATION REPORT



W-1a

FLOW TYPE	SURFACE	LENGTH (ft) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps)	Tc (min)
OVERLAND	GRS-DENSE	100	1.16	0.240	0.00	0.1	17.32
SHALLOW	UNPAVED	360	3.18	0.000	16.10	2.9	2.09
CHANNEL	NATRL TRAP (B=10,Y=6,SS=3:1)	4,961	1.26	0.050	68.56	7.7	10.72
BOX	7X5 RCB	263	0.81	0.014	136.50	12.3	0.36
		5,684					30.49

TIME LAG (min): 18.29

W-1b

FLOW TYPE	SURFACE	LENGTH (f	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps) Tc (min)
OVERLAND	GRS-DENSE	100	4.10	0.240	0.00	0.2	10.45
SHALLOW	UNPAVED	694	2.93	0.000	16.10	2.8	4.20
CHANNEL	NATRL TRAP (B=4,Y=3,SS=3:1)	1,287	2.20	0.050	42.29	6.3	3.42
		2,082					18.07

TIME LAG (min): 10.84

W-1c

FLOW TYPE	SURFACE	LENGTH (f1	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fps)	Tc (min)
OVERLAND	GRS-DENSE	100	0.50	0.240	0.00	0.1	24.25
SHALLOW	UNPAVED	333	0.61	0.000	16.10	1.3	4.43
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	1,239	1.74	0.050	28.69	3.8	5.45
		1,671					34.12

TIME LAG (min): 20.47

W-1d

FLOW TYPE	SURFACE	LENGTH (ft	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps)	Tc (min)
OVERLAND	GRS-DENSE	100	1.40	0.240	0.00	0.1	16.05
SHALLOW	UNPAVED	42	0.50	0.000	16.10	1.1	0.62
PIPE	42" RCP	2,244	1.09	0.014	97.10	10.2	3.68
CHANNEL	NATRL TRAP (B=4,Y=3,SS=3:1)	673	2.65	0.050	42.29	6.9	1.63
		3,059					21.98

TIME LAG (min): 13.19

W-1e

FLOW TYPE	SURFACE	LENGTH (ft	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fp	s) Tc (min)
OVERLAND	GRS-DENSE	100	0.50	0.240	0.00	0.1	24.25
SHALLOW	PAVED	423	0.63	0.000	20.30	1.6	4.39
SHALLOW	UNPAVED	223	0.50	0.000	16.10	1.1	3.26
PIPE	36" RCP	1,952	0.50	0.014	87.62	6.2	5.25
CHANNEL	NATRL TRAP (B=4,Y=3,SS=3:1)	546	3.53	0.050	42.29	7.9	1.14
		3,243					38.30

TIME LAG (min): 22.98

W-1f

FLOW TYPE	SURFACE	LENGTH (fl	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fps)	Tc (min)
OVERLAND	GRS-DENSE	100	0.50	0.240	0.00	0.1	24.25
SHALLOW	UNPAVED	1,253	0.83	0.000	16.10	1.5	14.28
PIPE	42" RCP	1,900	1.04	0.014	97.10	9.9	3.20
CHANNEL	NATRL TRAP (B=4,Y=3,SS=3:1)	88	2.24	0.050	42.29	6.3	0.23
		3,341					41.96
							05 4 0

TIME LAG (min): 25.18

W-1g

SHALLOW UNPAVED 1,099 2.61 0.000 16.10 2.6 7.04 CHANNEL NATRL TRAP (B=0,Y=2,SS=3:1) 2,432 1.22 0.050 28.69 3.2 12.80	FLOW TYPE	SURFACE	LENGTH (ft) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps) Tc (min)
CHANNEL NATRL TRAP (B=0,Y=2,SS=3:1) 2,432 1.22 0.050 28.69 3.2 12.80	OVERLAND	GRS-DENSE	100	1.43	0.240	0.00	0.1	15.93
	SHALLOW	UNPAVED	1,099	2.61	0.000	16.10	2.6	7.04
3 631 35 77	CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	2,432	1.22	0.050	28.69	3.2	12.80
5,051 55.77			3,631					35.77

TIME LAG (min): 21.46

W-2a

FLOW TYPE	SURFACE	length (f	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps)) Tc (min)
OVERLAND	GRS-DENSE	100	1.43	0.240	0.00	0.1	15.91
PIPE	30" RCP	132	0.50	0.014	77.59	5.5	0.40
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	821	0.81	0.050	28.69	2.6	5.29
		1,053					21.60

TIME LAG (min): 12.96

W-3a

FLOW TYPE	SURFACE	LENGTH (ft) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fp:	s) Tc (min)
OVERLAND	GRS-DENSE	100	6.10	0.240	0.00	0.1	13.68
SHALLOW	UNPAVED	434	4.03	0.000	16.10	3.2	2.24
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	1,430	1.62	0.050	28.69	3.7	6.52
BOX	5X5 RCB	72	0.99	0.014	123.17	12.3	0.10
		2,036					22.54

TIME LAG (min): 13.52

W-3b

FLOW TYPE	SURFACE	LENGTH (f	t) SLOPE (%)	ROUGHNESS	k value	VELOCITY (fp	s) Tc (min)
OVERLAND	GRS-DENSE	100	5.39	0.240	0.00	0.2	9.69
CHANNEL	NATRL TRAP (B=0,Y=2,SS=3:1)	565	5.50	0.050	28.69	6.7	1.40
		665					11.09

TIME LAG (min): 6.65

W-4a

FLOW TYPE	SURFACE	LENGTH (f1	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fp:	s) Tc (min)
OVERLAND	GRS-DENSE	100	1.99	0.240	0.00	0.1	21.43
SHALLOW	UNPAVED	429	3.90	0.000	16.10	3.2	2.25
CHANNEL	NATRL TRAP (B=6,Y=4,SS=3:1)	1,150	1.65	0.050	51.79	6.6	2.88
BOX	7X5 RCB	46	1.72	0.014	136.50	17.9	0.04
		1,726					26.60

TIME LAG (min): 15.96

W-4b

FLOW TYPE	SURFACE	LENGTH (fi	t) SLOPE (%)	ROUGHNESS	K VALUE	VELOCITY (fps)	Tc (min)
OVERLAND	GRS-DENSE	100	2.22	0.240	0.00	0.1	20.52
SHALLOW	UNPAVED	777	3.94	0.000	16.10	3.2	4.05
CHANNEL	NATRL TRAP (B=4,Y=3,SS=3:1)	1,714	3.73	0.050	42.29	8.2	3.50
		2,591					28.07

TIME LAG (min): 16.84

SCS Hydrologic Parameters

PRE PROJECT HYDROLOGIC PARAMETERS REPORT

BASIN ID	BASIN AREA (acres)	Tc (minutes)	TL (minutes)	COMPOSITE CN
W-1a	118.6	30.5	18.3	78.4
W-1b	71.5	18.1	10.8	78.5
W-1c	23.6	34.1	20.5	93.2
W-1d	30.4	22.0	13.2	93.9
W-1e	98.2	38.3	23.0	93.2
W-1f	135.6	42.0	25.2	93.1
W-1g	107.9	35.8	21.5	85.4
W-2a	16.1	21.6	13.0	74.2
W-3a	30.8	22.5	13.5	66.4
W-3b	9.0	11.1	6.7	80.1
W-4a	41.4	26.6	16.0	68.7
W-4b	68.9	16.8	10.1	80.3

POST PROJECT HYDROLOGIC PARAMETERS REPORT

BASIN ID	BASIN AREA (acres)	Tc (minutes)	TL (minutes)	COMPOSITE CN
W-1a	118.6	10.0	6.0	94.5
W-1b	71.5	10.0	6.0	90.7
W-1c	23.6	34.1	20.5	93.2
W-1d	30.4	22.0	13.2	93.9
W-1e	98.2	38.3	23.0	93.2
W-1f	135.6	42.0	25.2	93.1
W-1g	107.9	35.8	21.5	85.4
W-2a	16.1	10.0	6.0	94.2
W-3a	30.8	10.0	6.0	93.0
W-3b	9.0	10.0	6.0	90.0
W-4a	41.4	10.0	6.0	93.4
W-4b	68.9	10.0	6.0	90.1

Weighted C Factor Calculations

EXISTING WEIGHTED C FACTOR CALCULATIONS

BASIN ID	C FACTOR	AREA (acres)	% AREA	WEIGHTED C FACTOR
E-01	0.95	1.7	21.4%	0.44
E-01	0.30	6.3	78.6%	0.44
	0.95	2.7	9.2%	
E-02	0.70	2.4	8.2%	0.39
	0.30	24.1	82.6%	
	0.95	0.5	3.7%	
E-03	0.70	5.2	40.3%	0.49
	0.30	7.3	56.0%	
	0.95	2.8	2.2%	
E-04	0.70	4.8	3.7%	0.30
L-04	0.15	23.7	18.5%	0.50
	0.30	96.9	75.6%	
	0.95	1.3	4.5%	
E-05	0.15	2.6	9.2%	0.32
	0.30	24.0	86.2%	
	0.95	2.8	26.4%	
E-06	0.15	0.9	8.9%	0.46
	0.30	6.9	64.7%	
	0.95	2.9	19.5%	
E-07	0.15	2.1	13.7%	0.45
	0.30	12.1	80.5%	
E-08	0.95	2.4	62.8%	0.65
E-06	0.15	1.4	37.2%	0.05
	0.95	4.7	2.8%	
E-09	0.15	109.6	65.7%	0.22
	0.30	52.5	31.5%	
E-10	0.95	0.7	35.0%	0.43
	0.15	1.2	65.0%	0.70

PROPOSED WEIGHTED C FACTOR CALCULATIONS

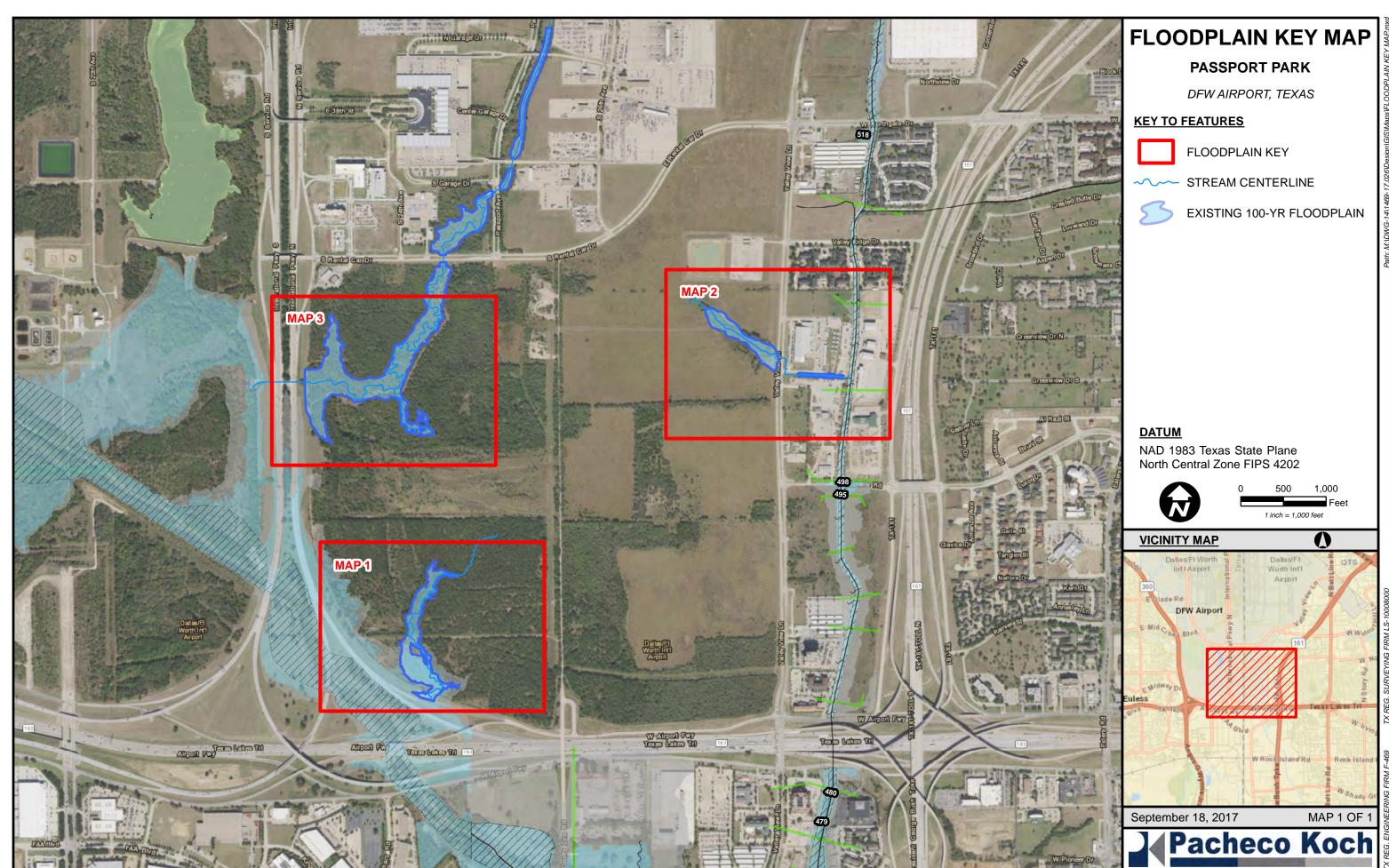
BASIN ID	C FACTOR	AREA (acres)	% AREA	WEIGHTED C FACTOR	
E-01	0.95	1.7	21.4%	0.83	
E-01	0.80	6.3	78.6%	0.85	
E-02	0.95	2.7	9.2%	0.81	
E-02	0.80	26.5	90.7%	0.81	
E-03	0.95	0.5	3.7%	0.81	
E-05	0.80	12.5	96.4%	0.81	
E-04	0.95	2.8	2.2%	0.80	
E-04	0.80	125.3	97.8%	0.80	
E-05	0.95	1.3	4.5%	0.91	
E-05	0.80	26.6	95.5%	0.81	
E-06	0.95	2.8	26.4%	0.84	
L-00	0.80	7.8	73.6%	0.84	
E-07	0.95	2.9	19.5%	0.83	
207	0.80	12.1	80.5%	0.05	
E-08	0.95	2.4	62.8%	0.89	
L-00	0.80	1.4	37.2%	0.85	
E-09	0.95	4.7	2.8%	0.80	
L-09	0.80	162.2	97.2%	0.80	
E-10	0.95	0.7	35.0%	0.85	
L-10	0.80	1.2	65.0%	0.05	

Appendix B

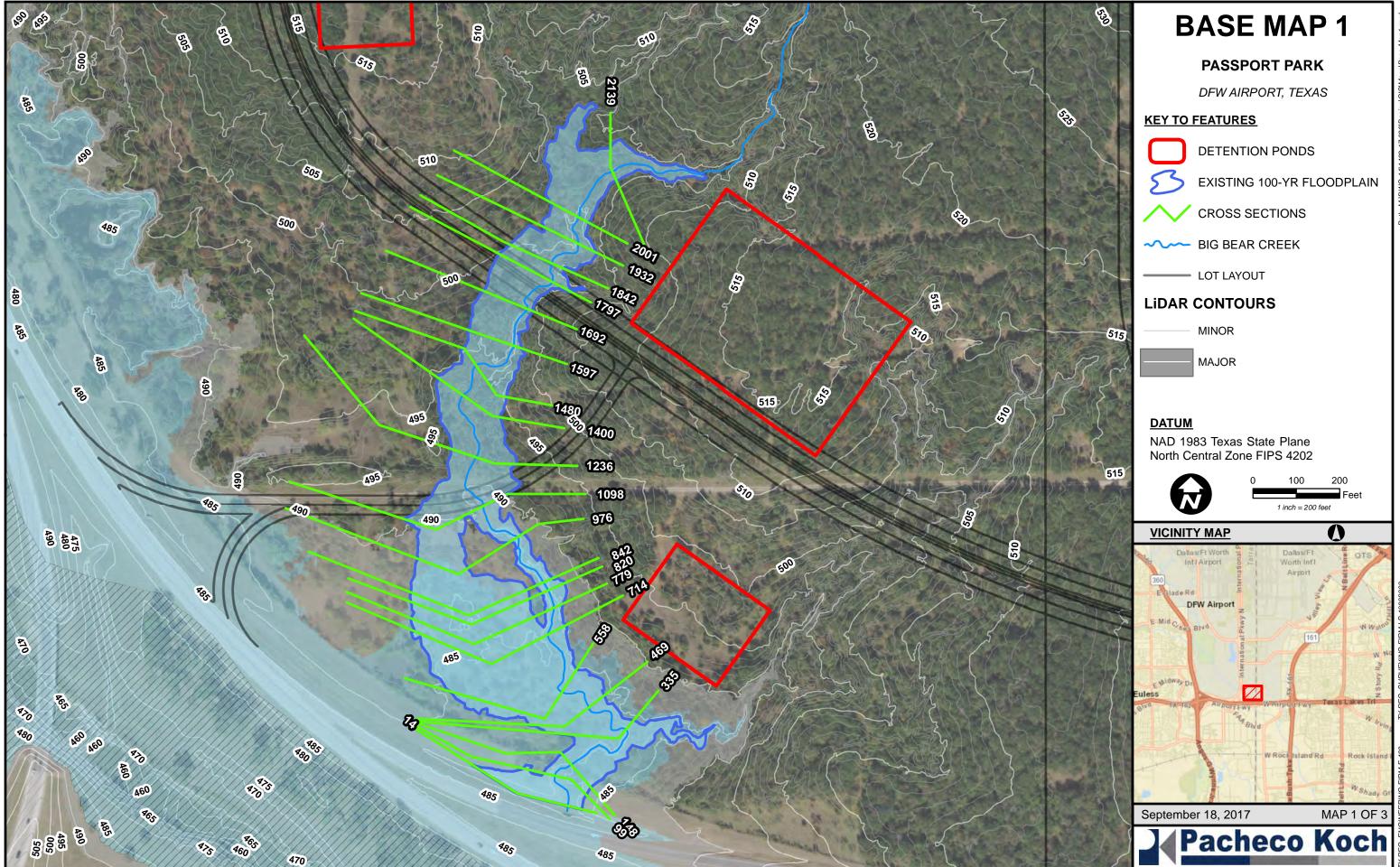
Hydraulics

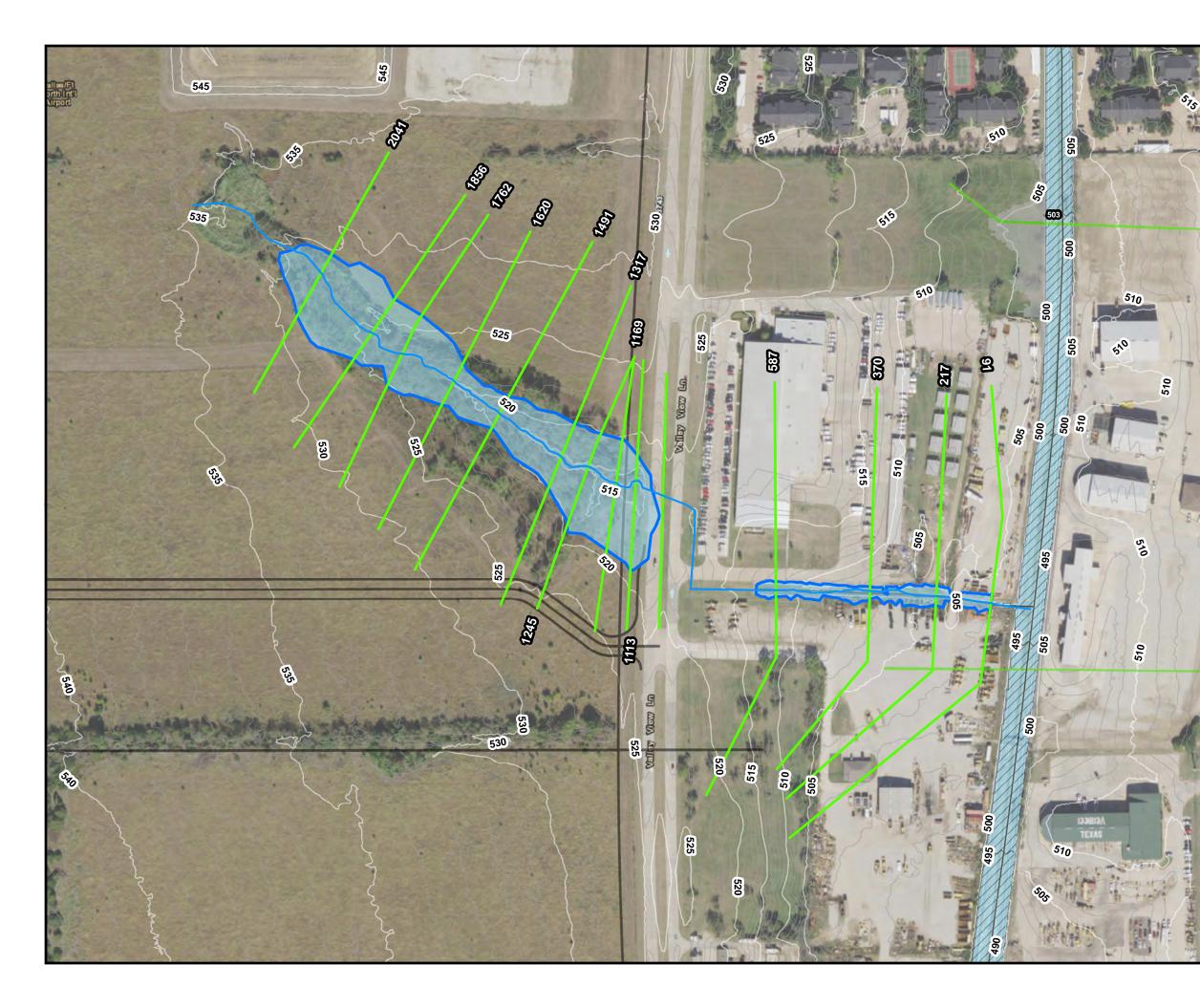
- Floodplain Key Map
- Floodplain Work Maps
- Cross-Section Plots
- Flood Profile
- Existing Conditions Model Output

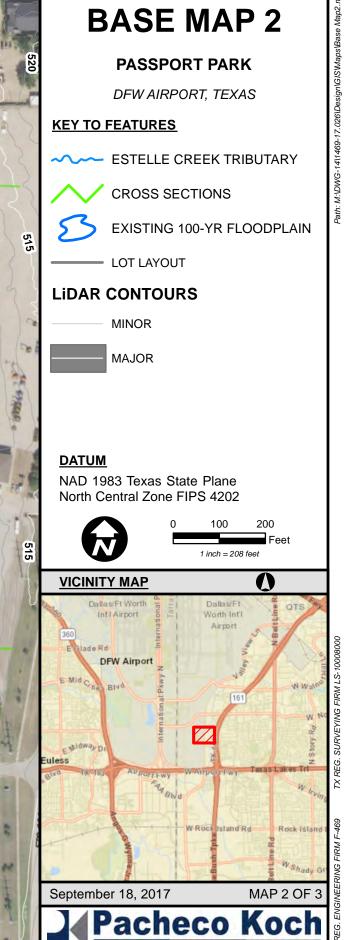
Floodplain Key Map

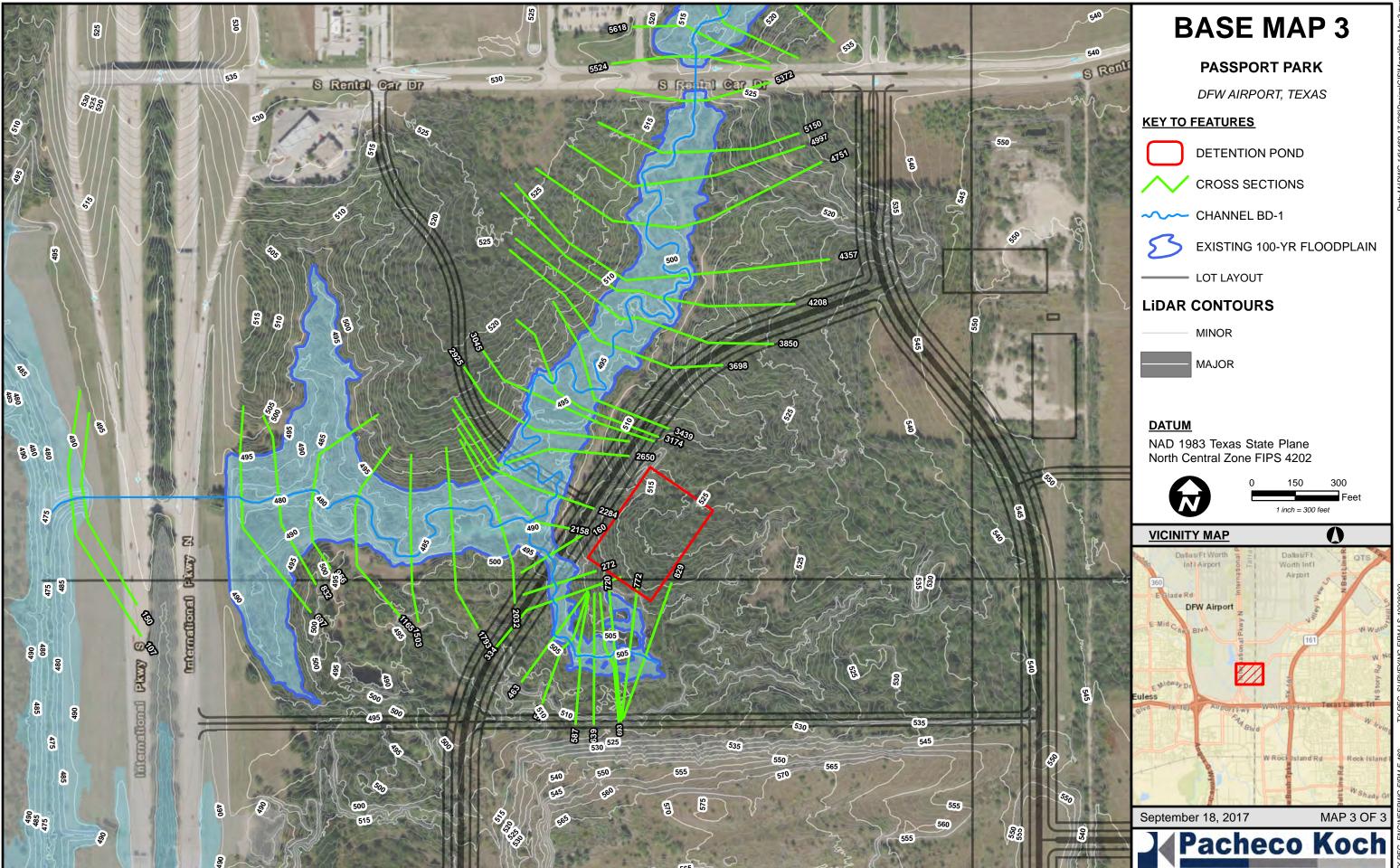


Floodplain Work Maps

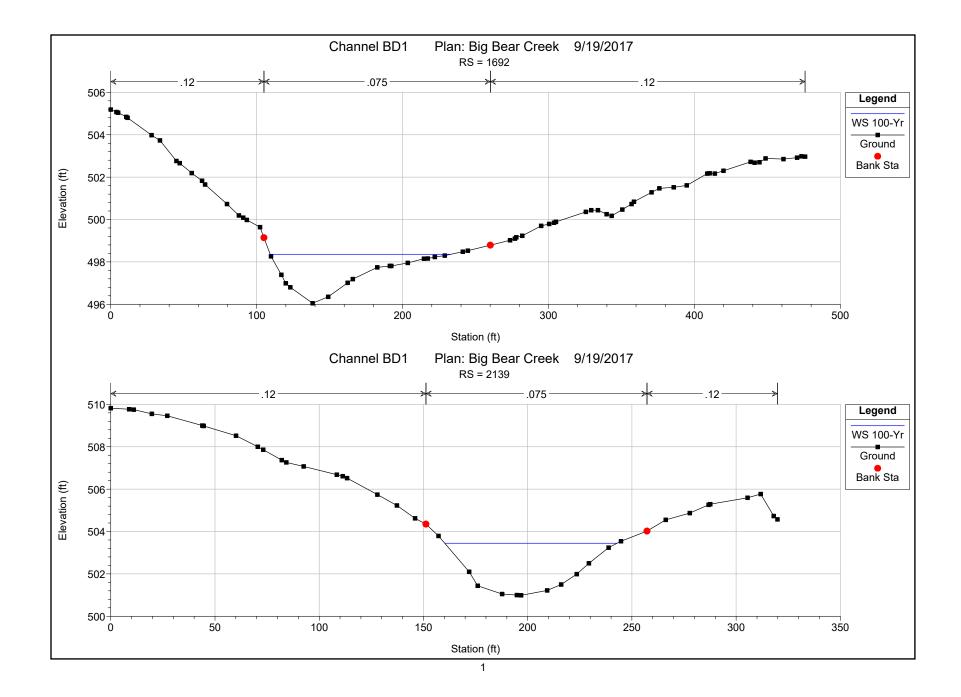


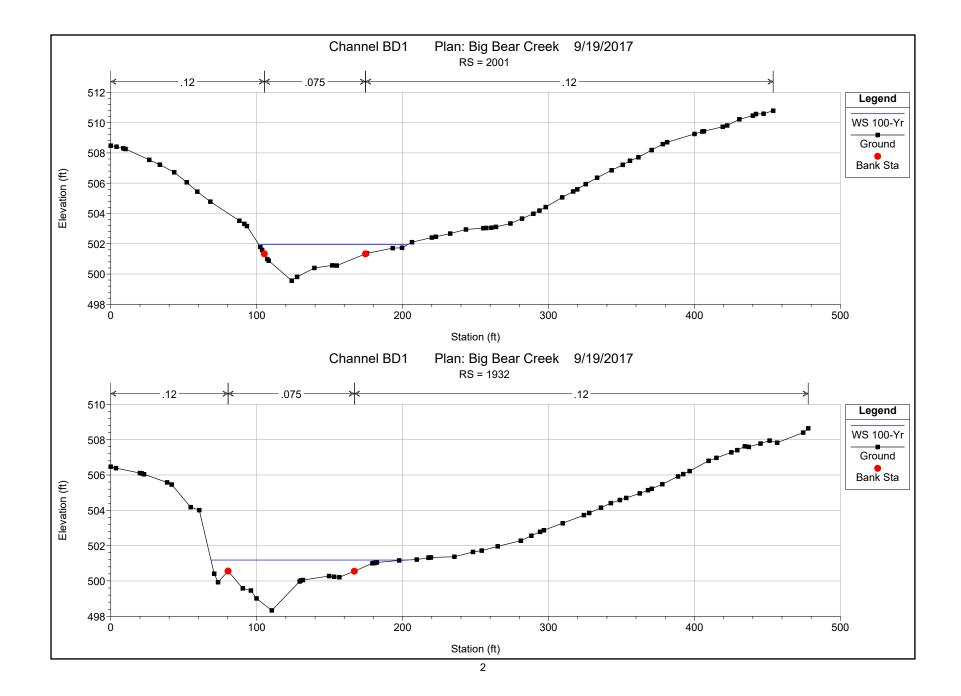


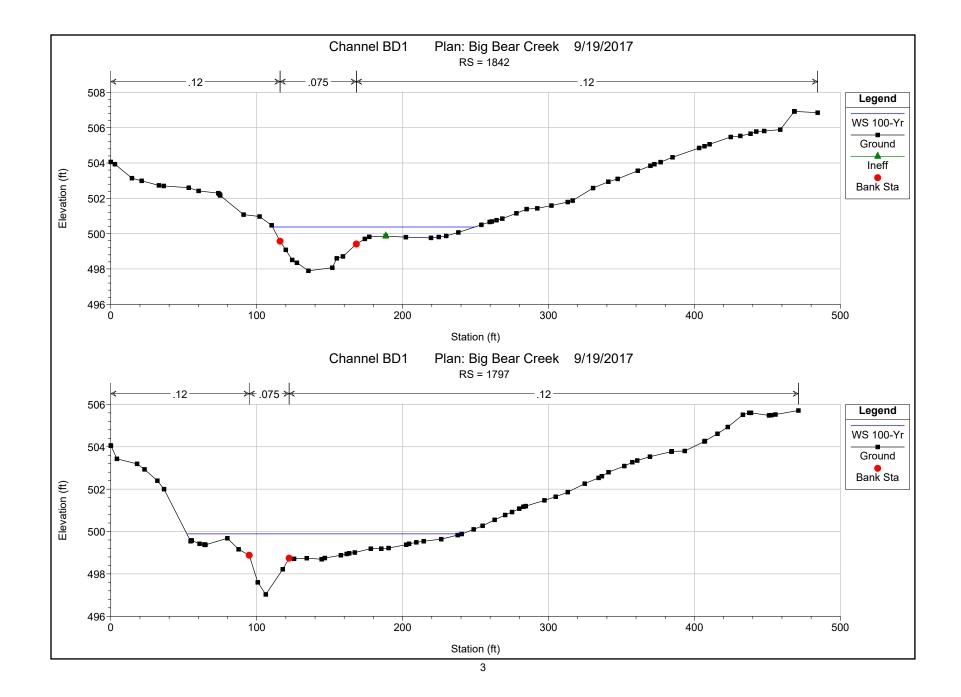


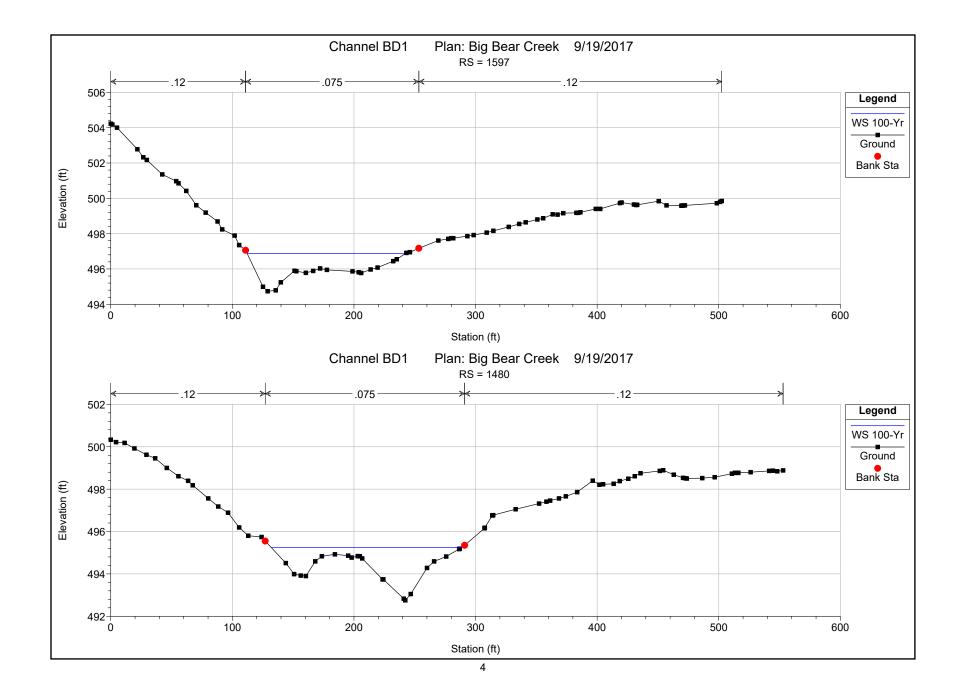


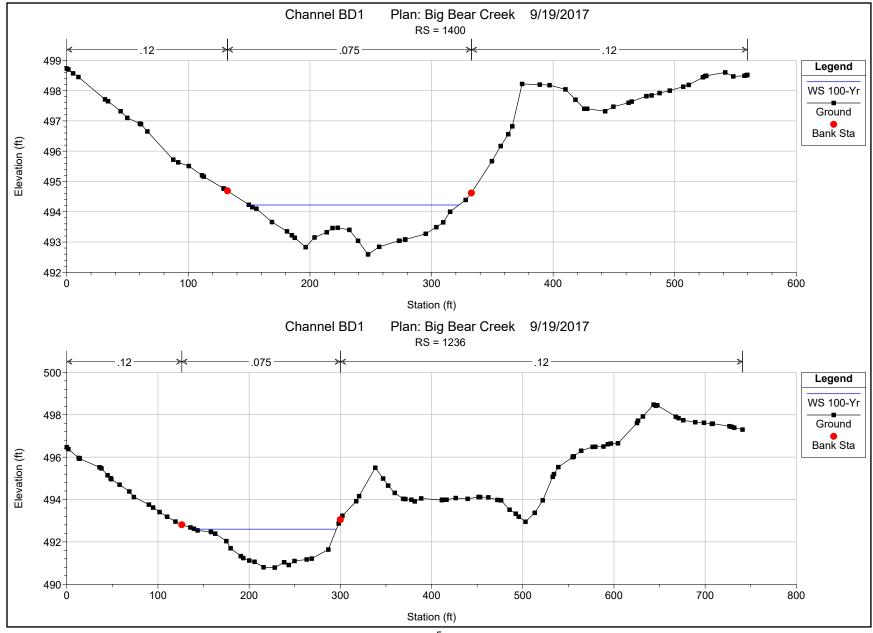
Cross-Section Plots

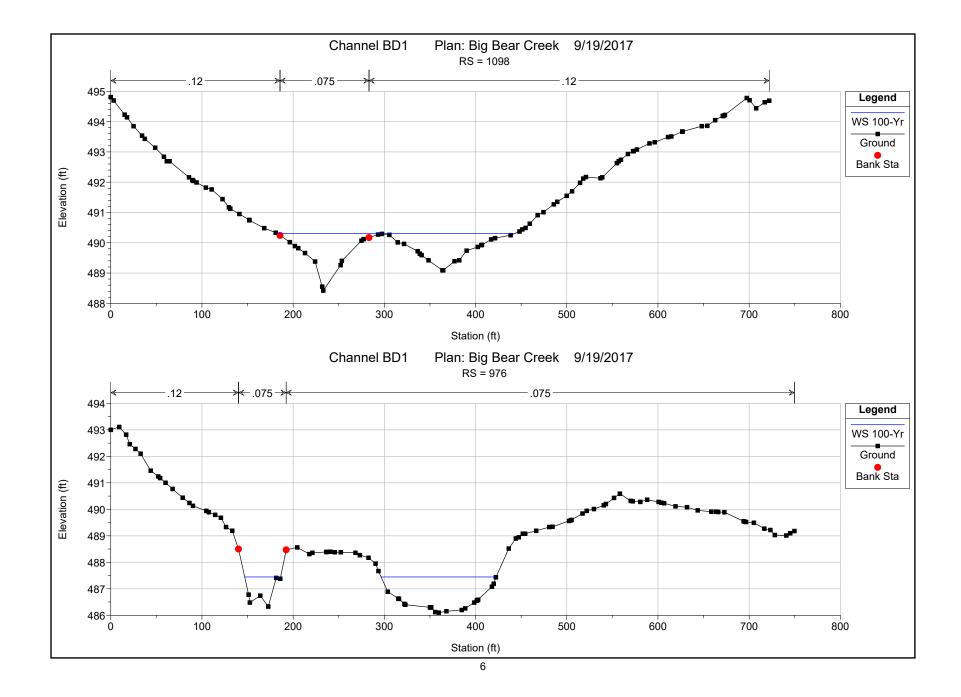


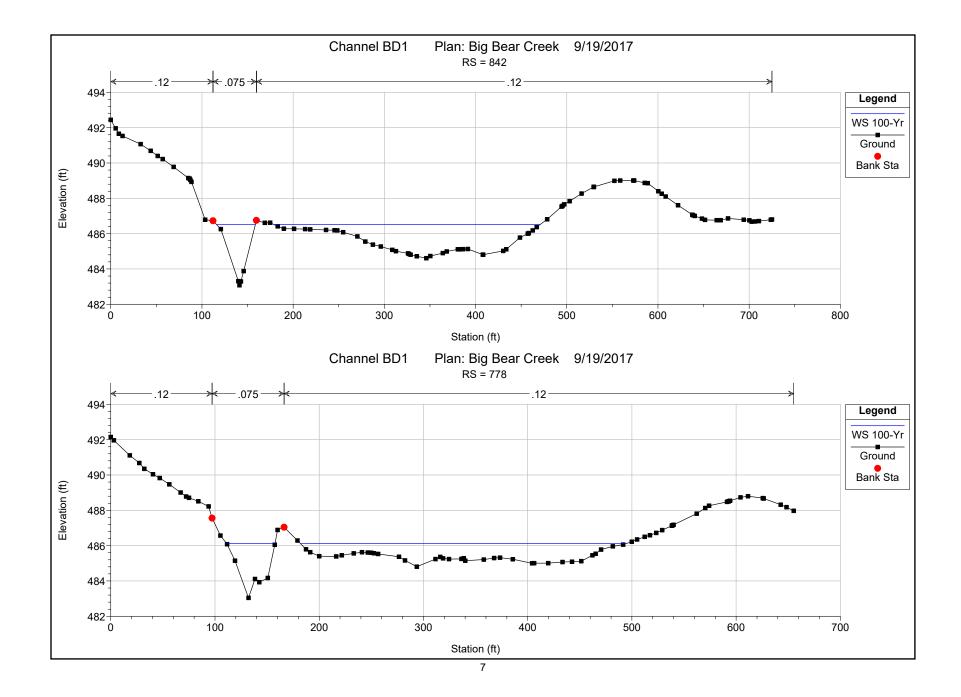


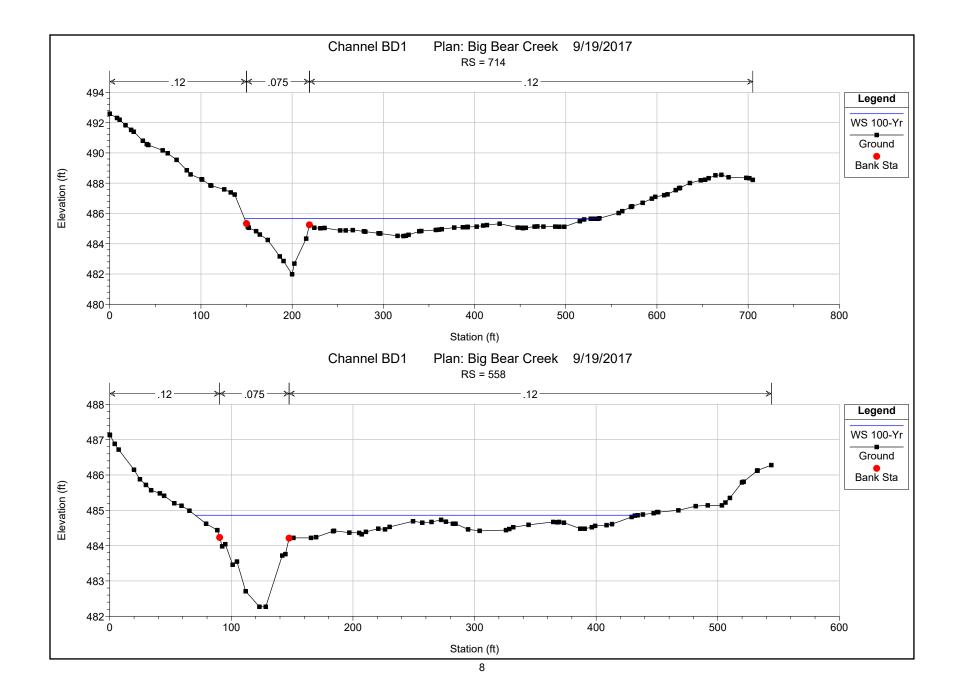


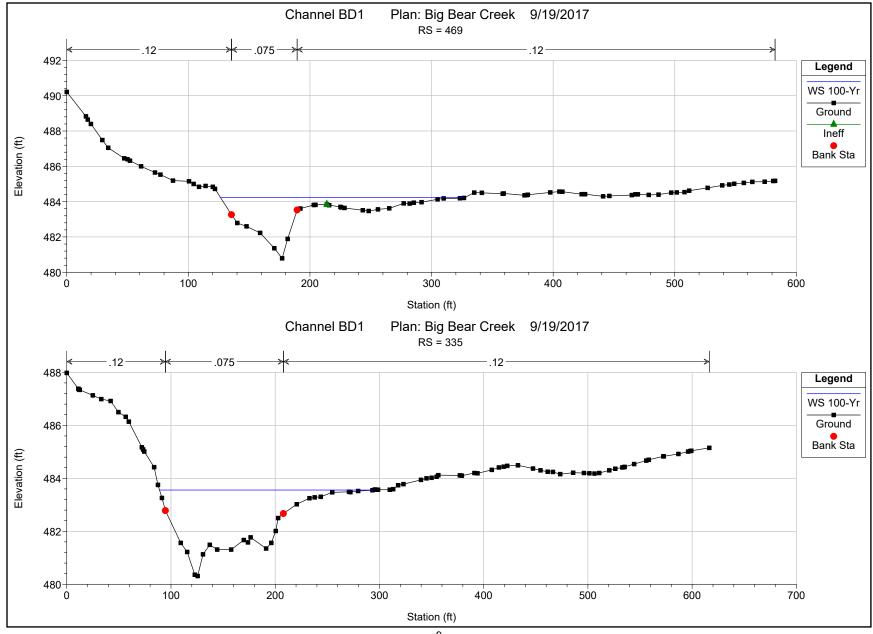


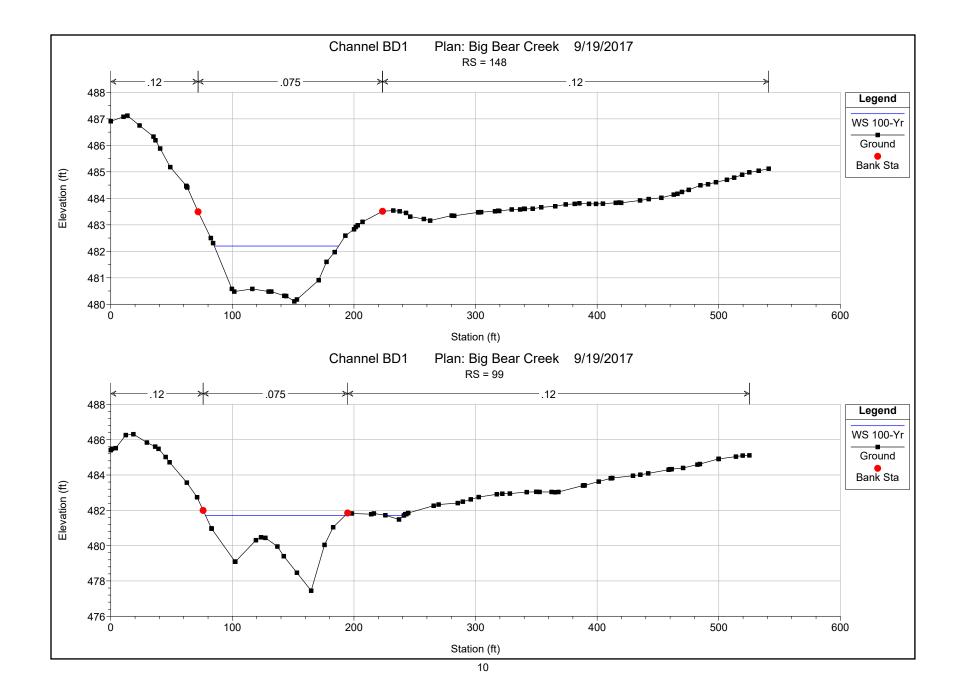


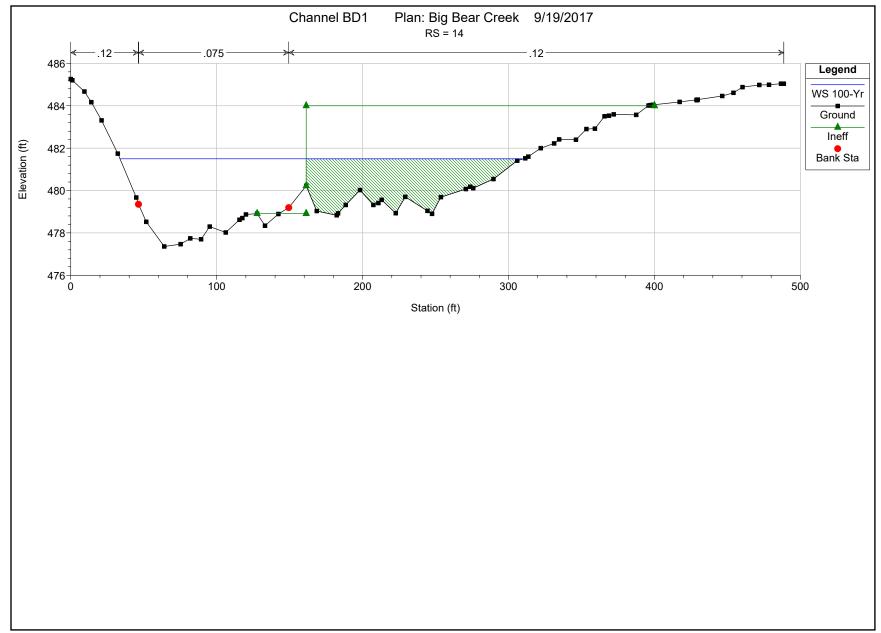


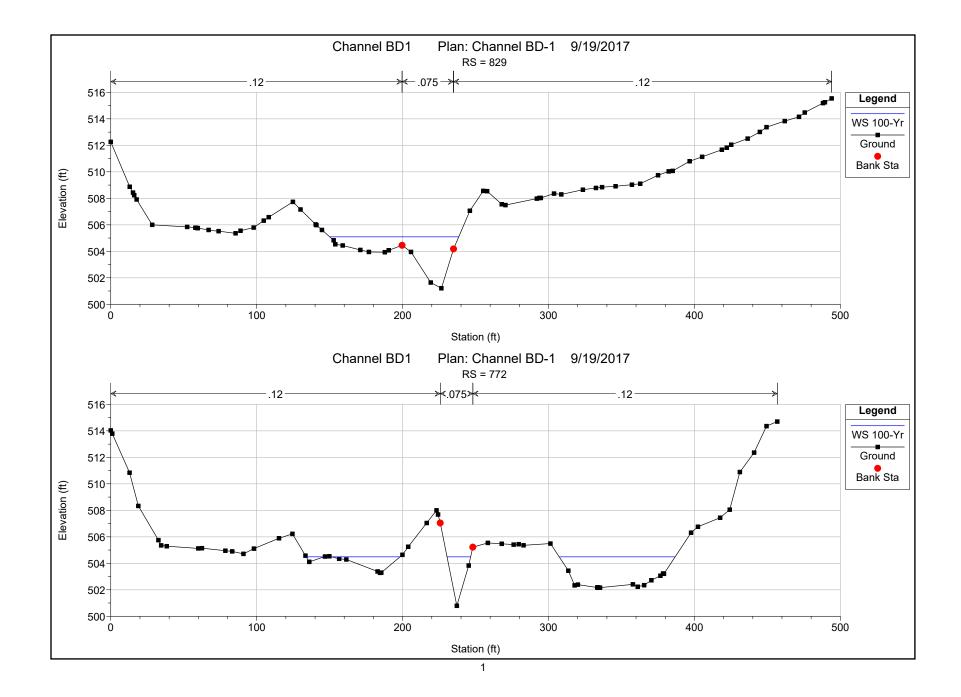


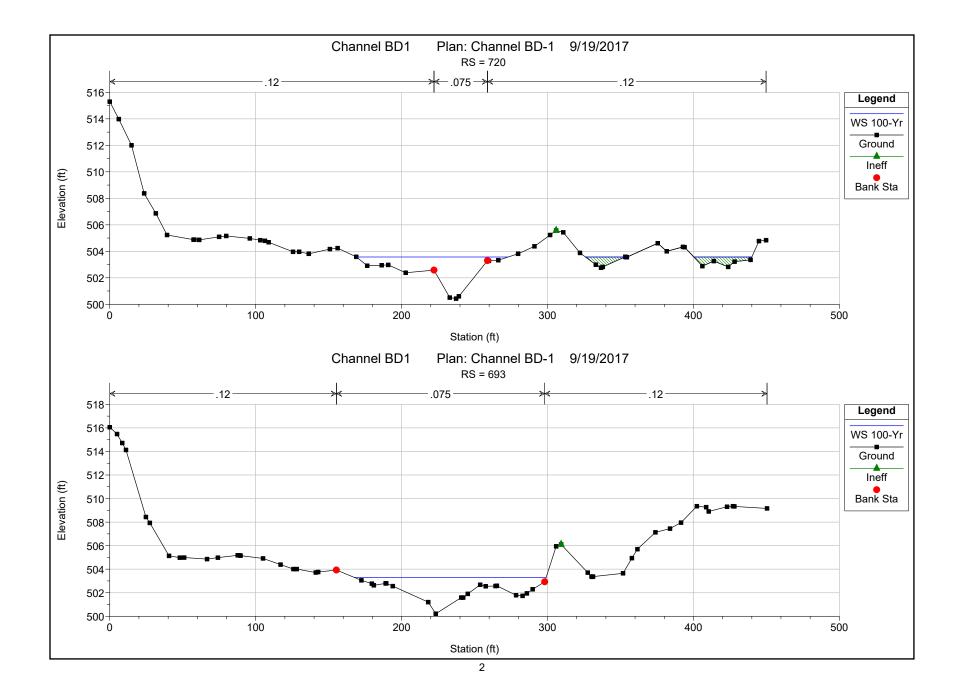


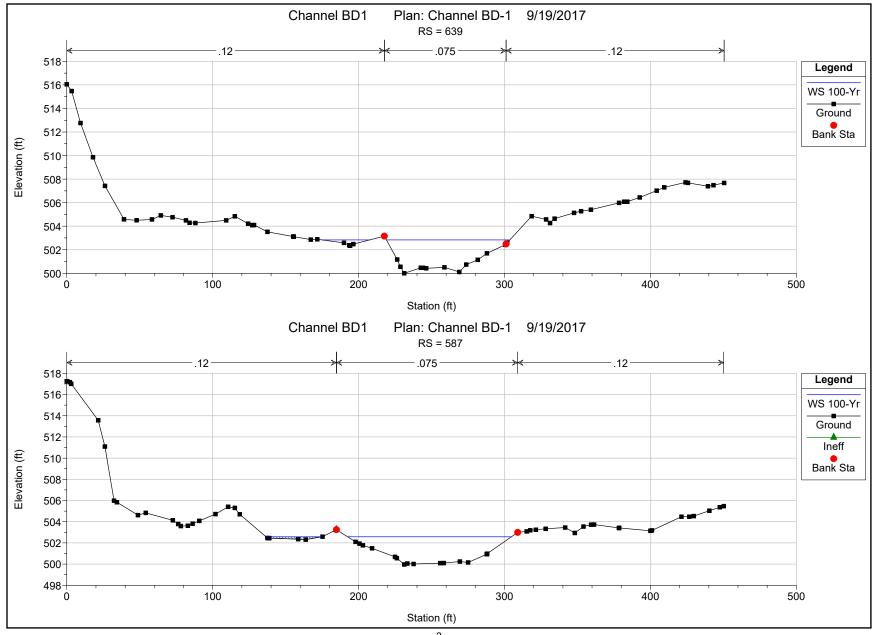


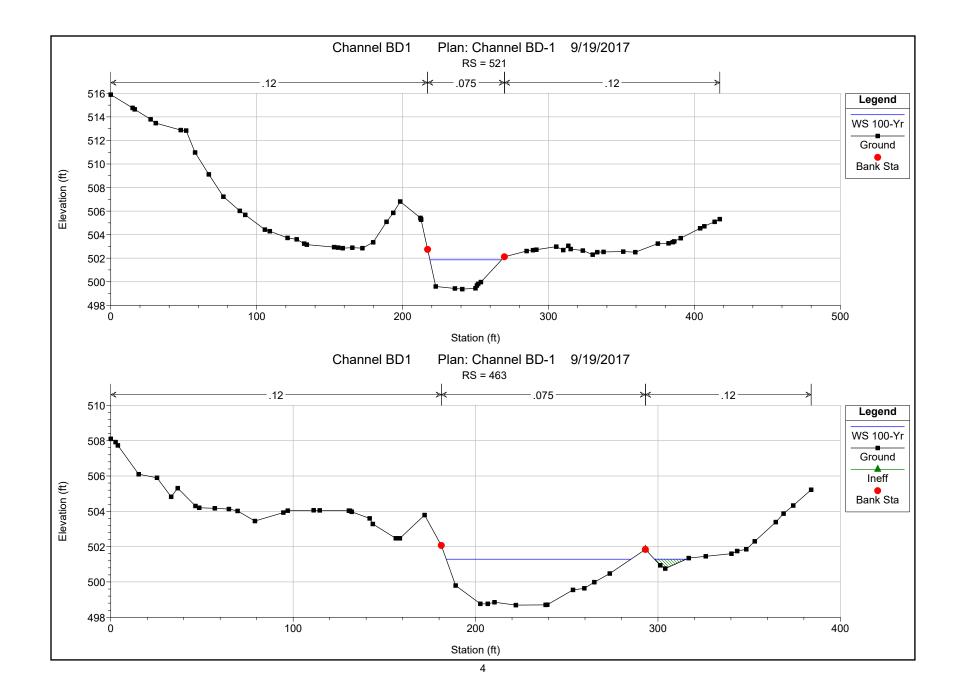


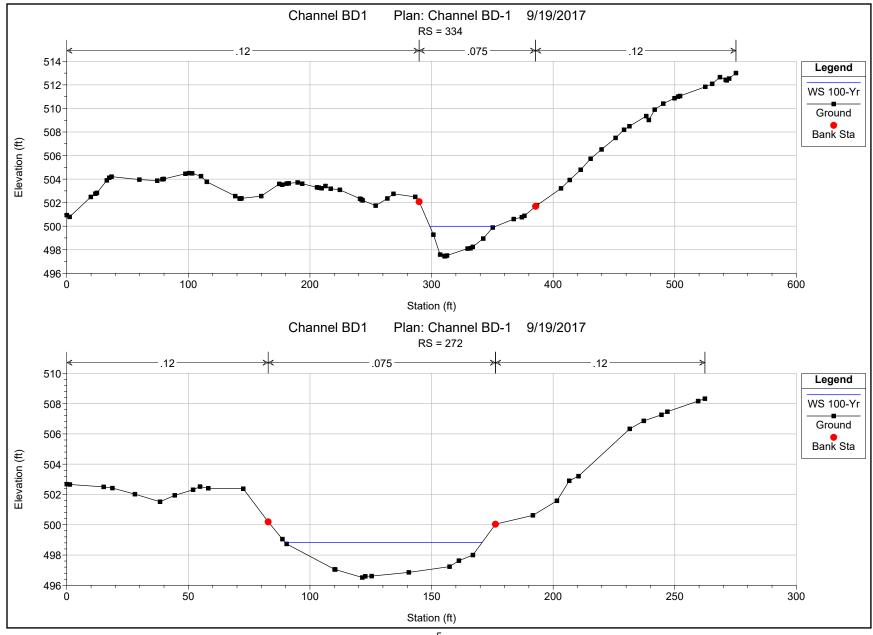


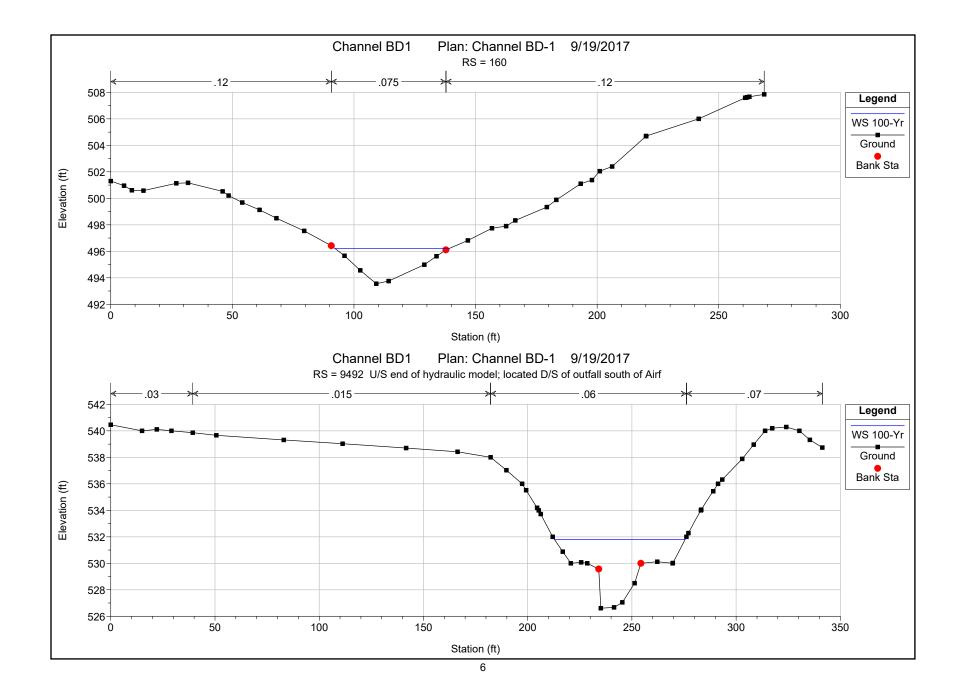


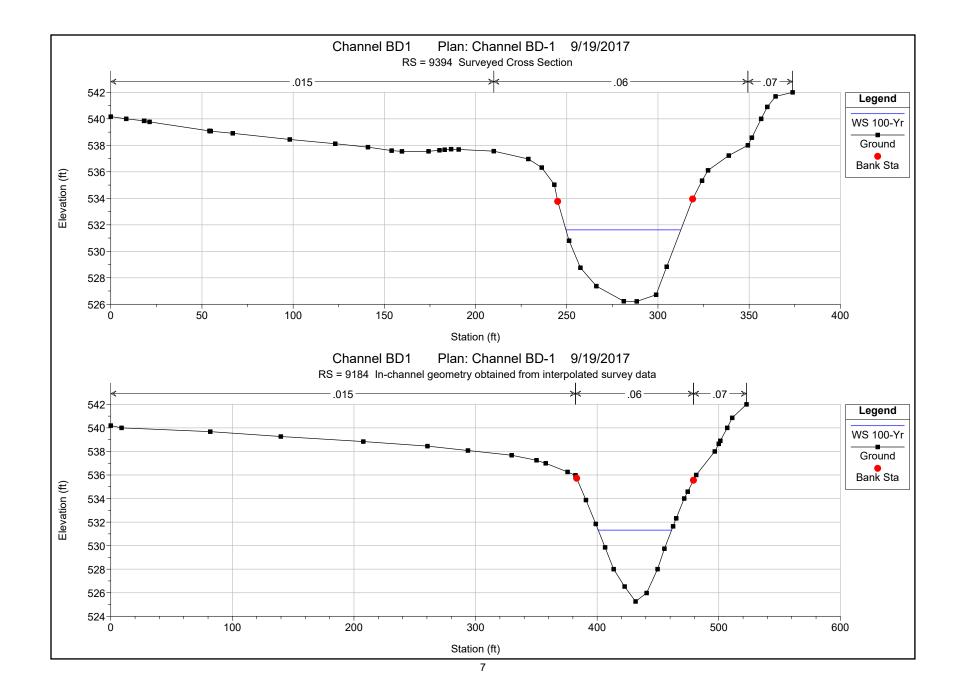


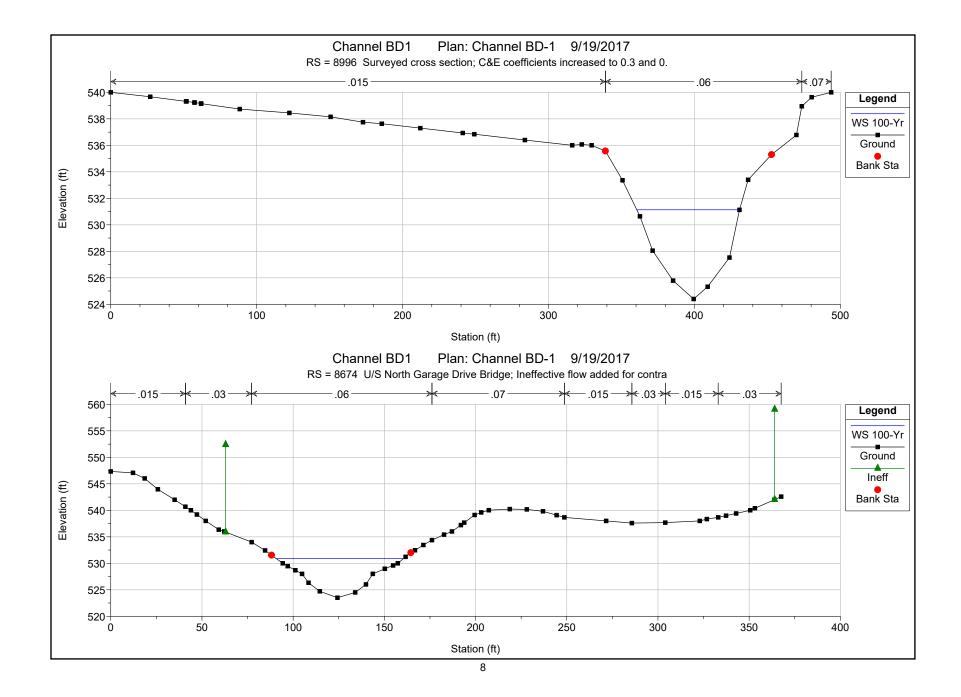


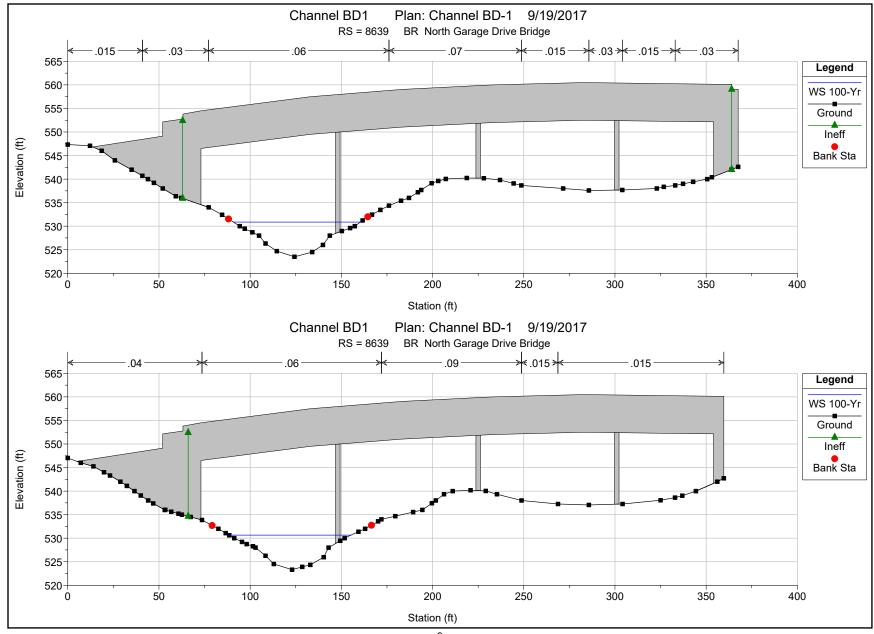


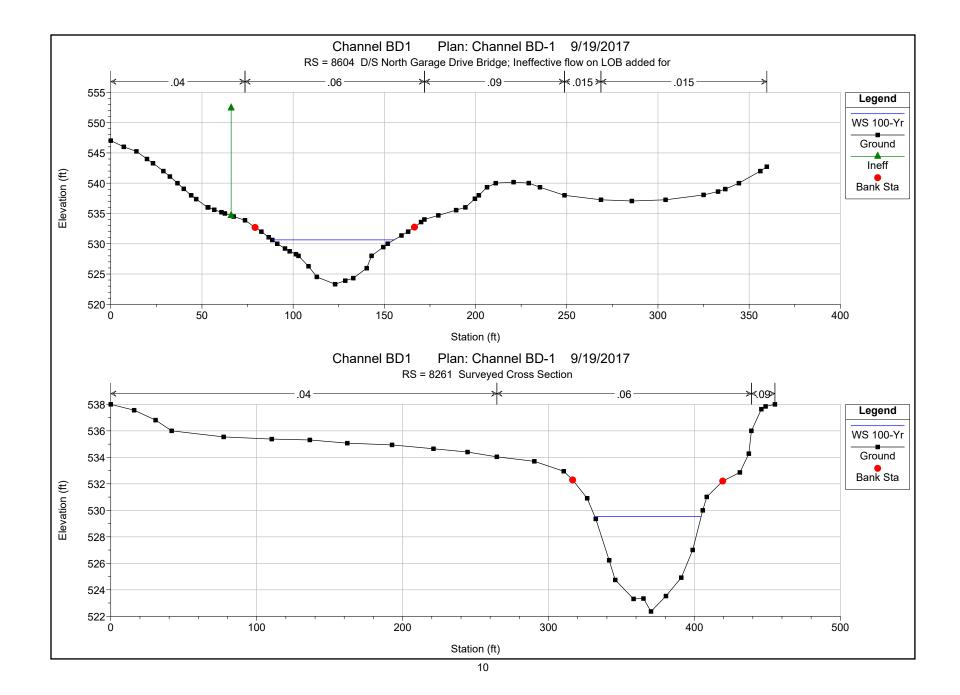


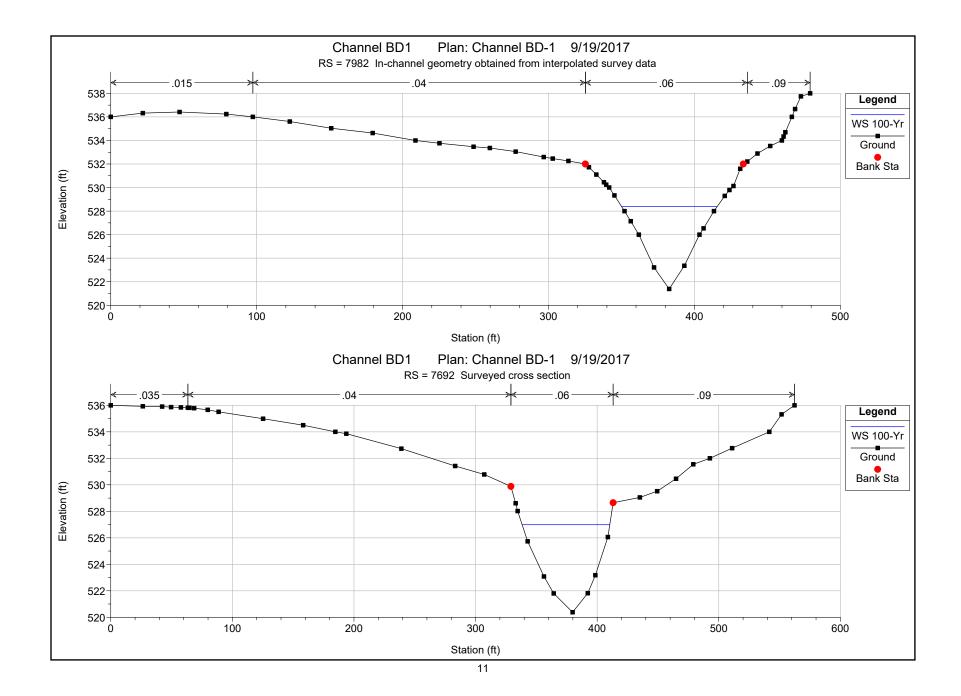


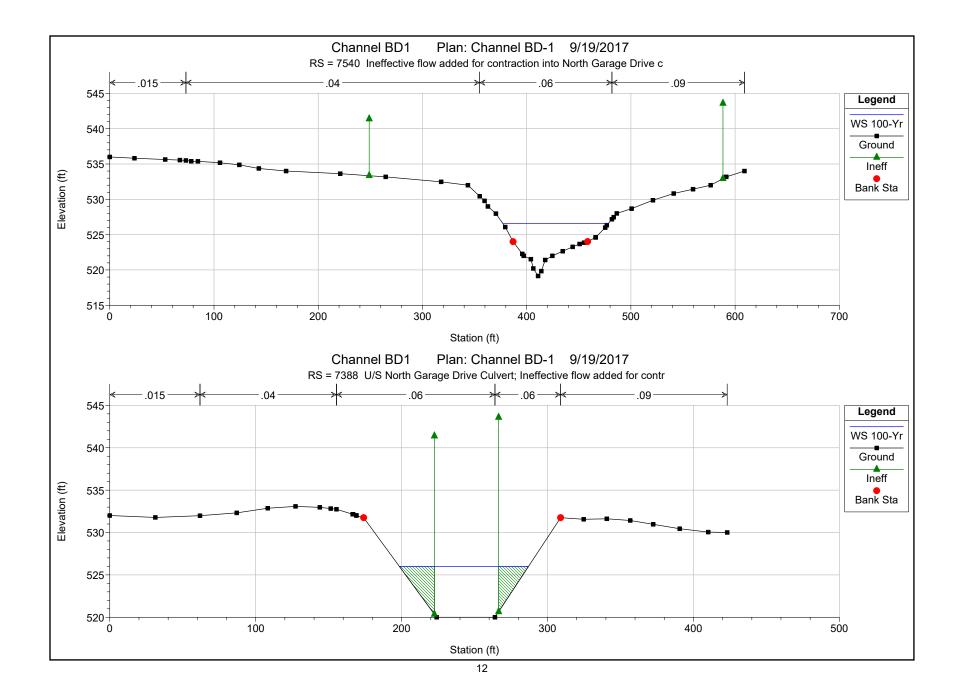


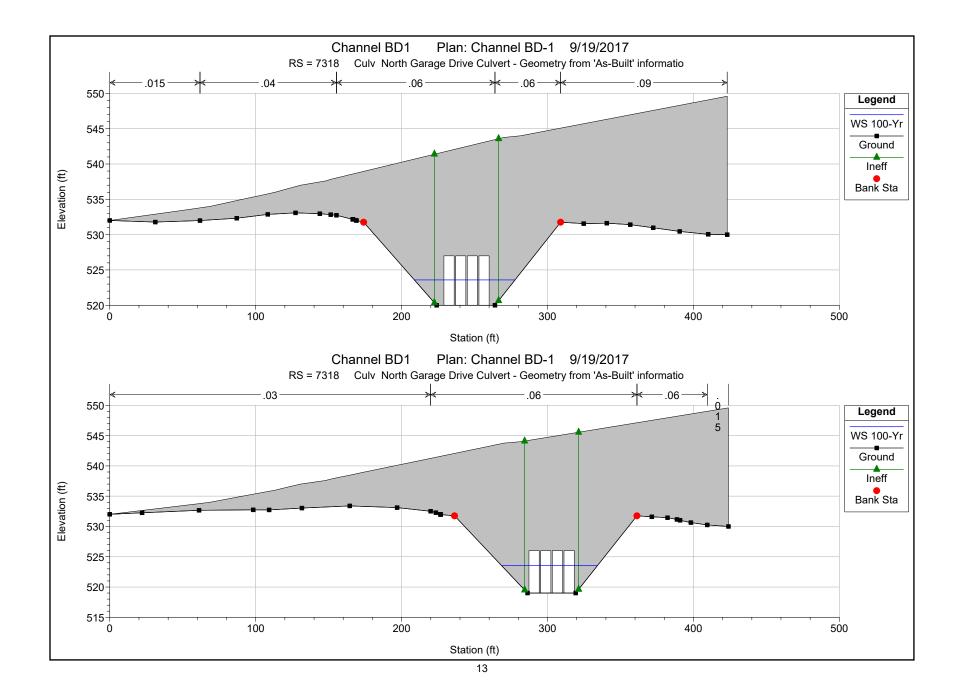


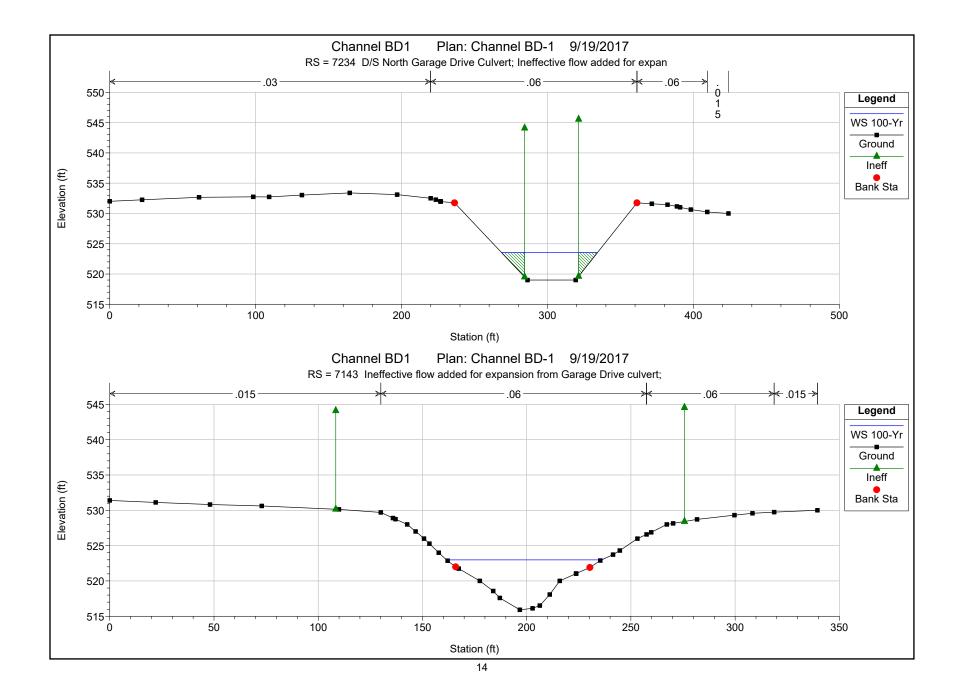


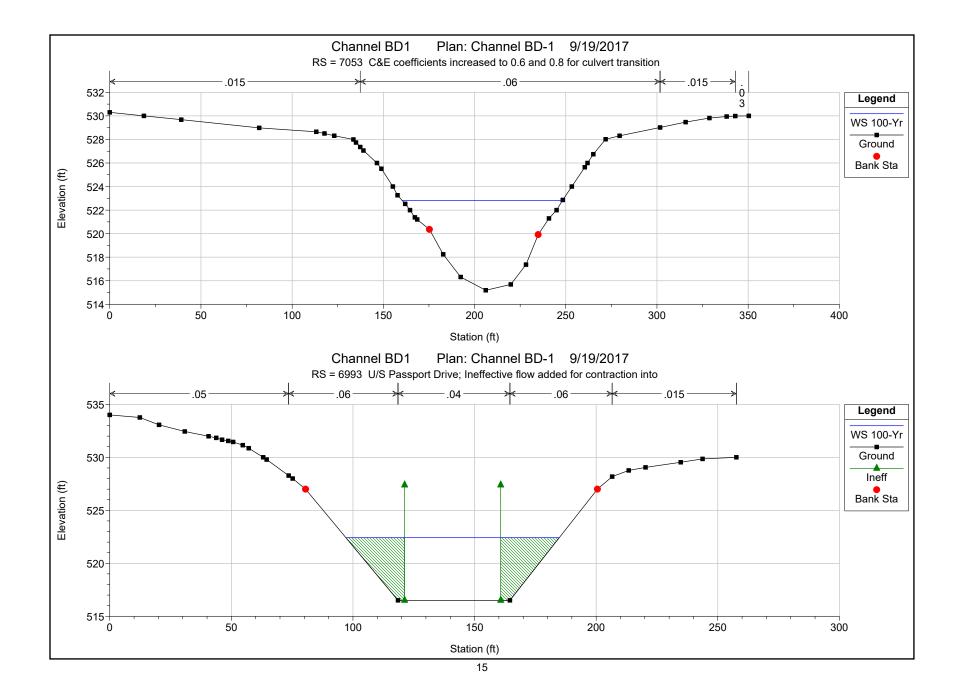


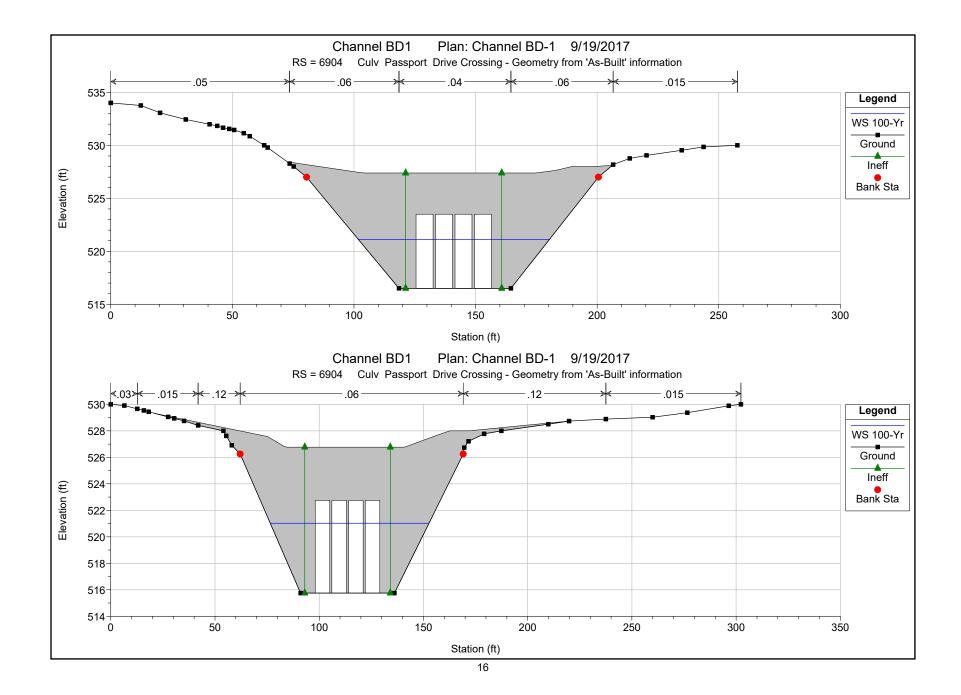


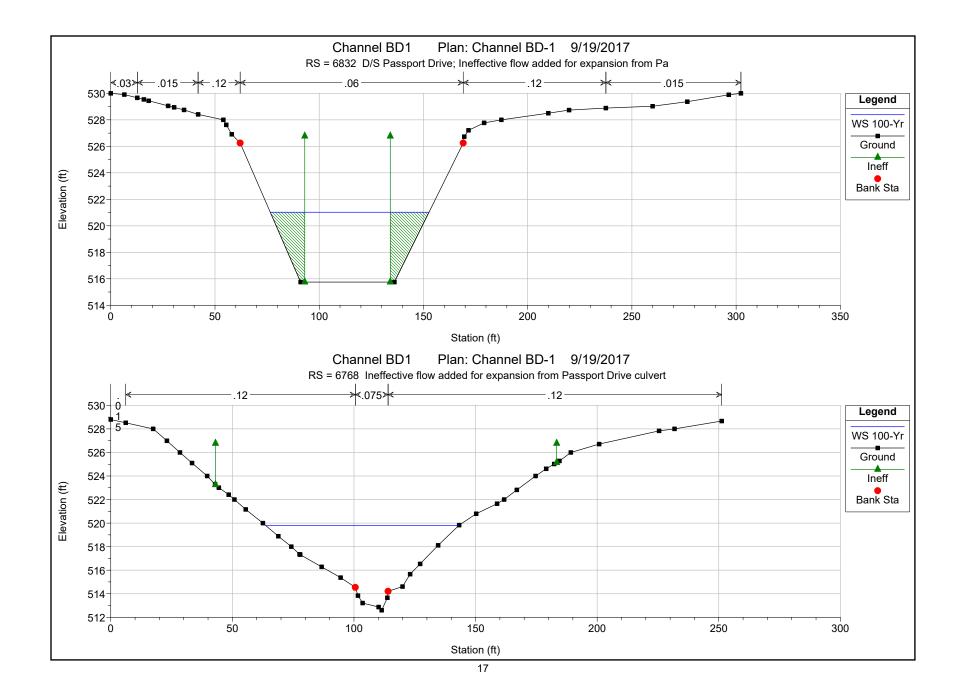


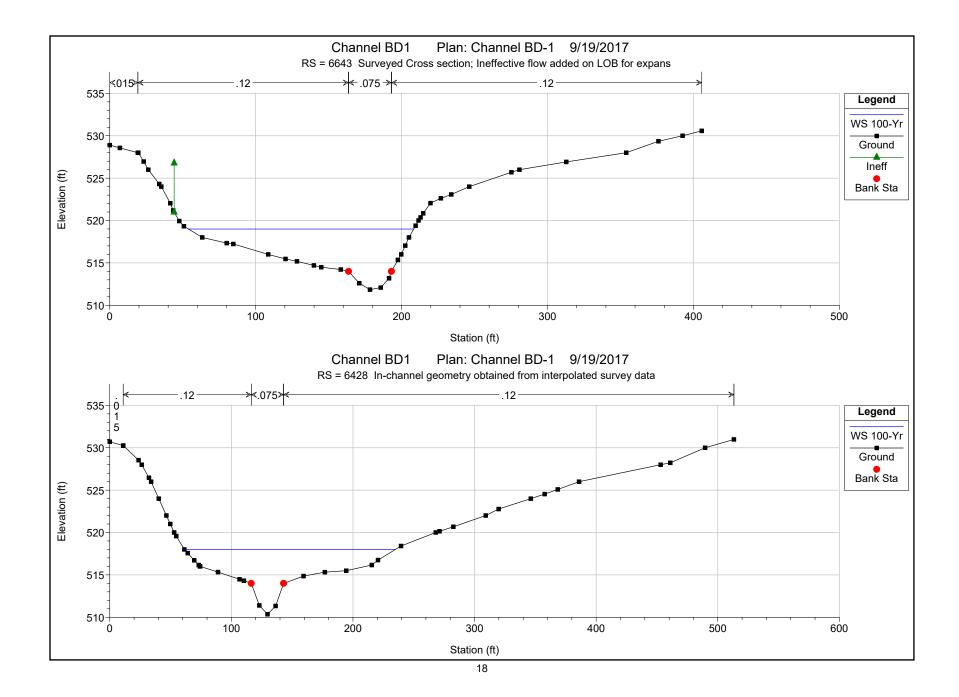


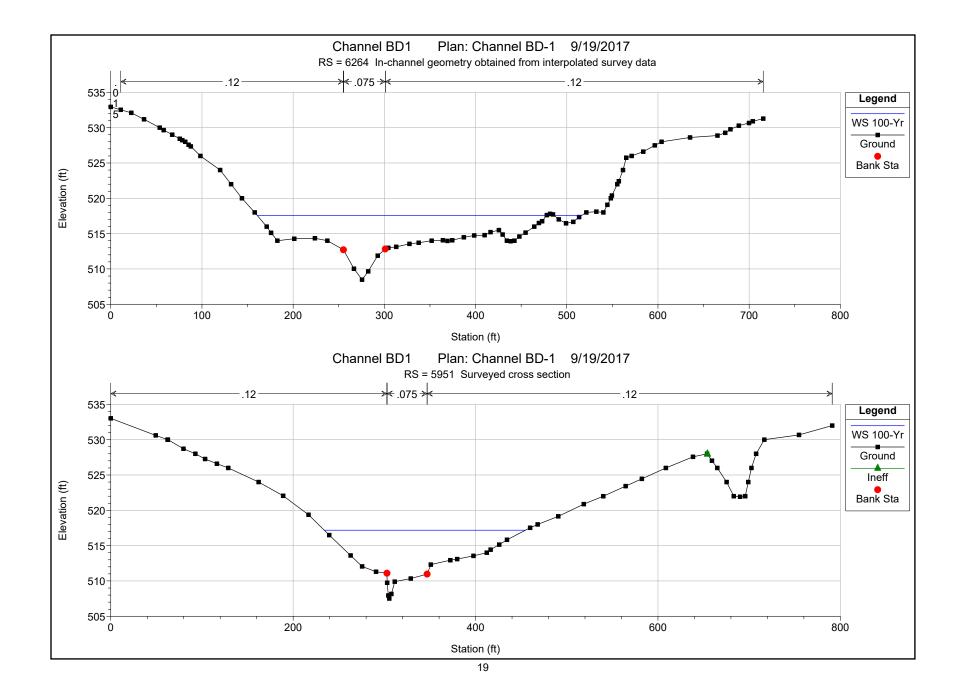


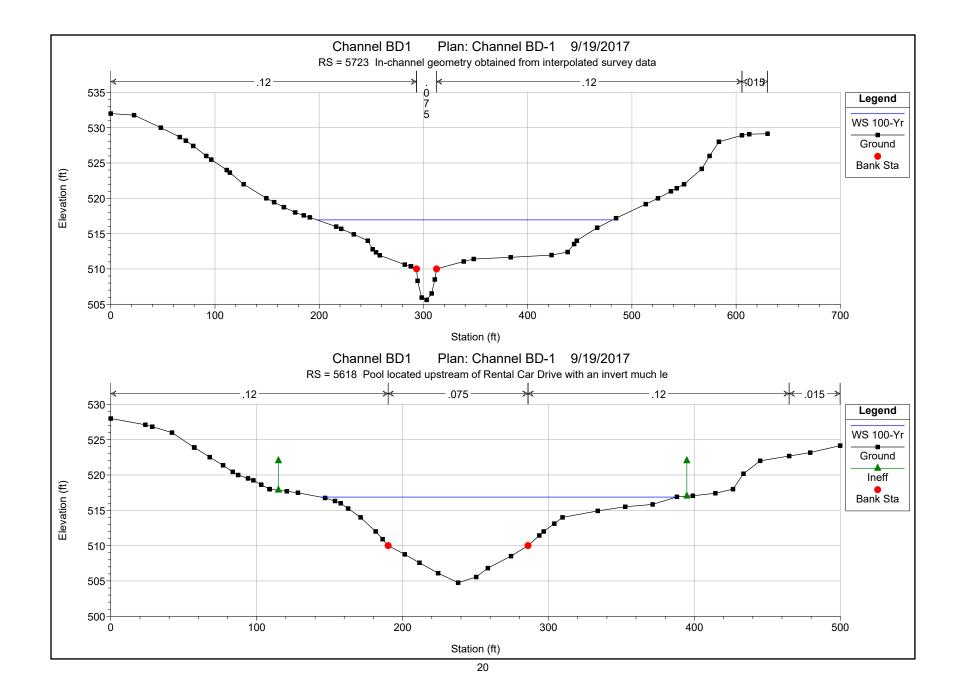


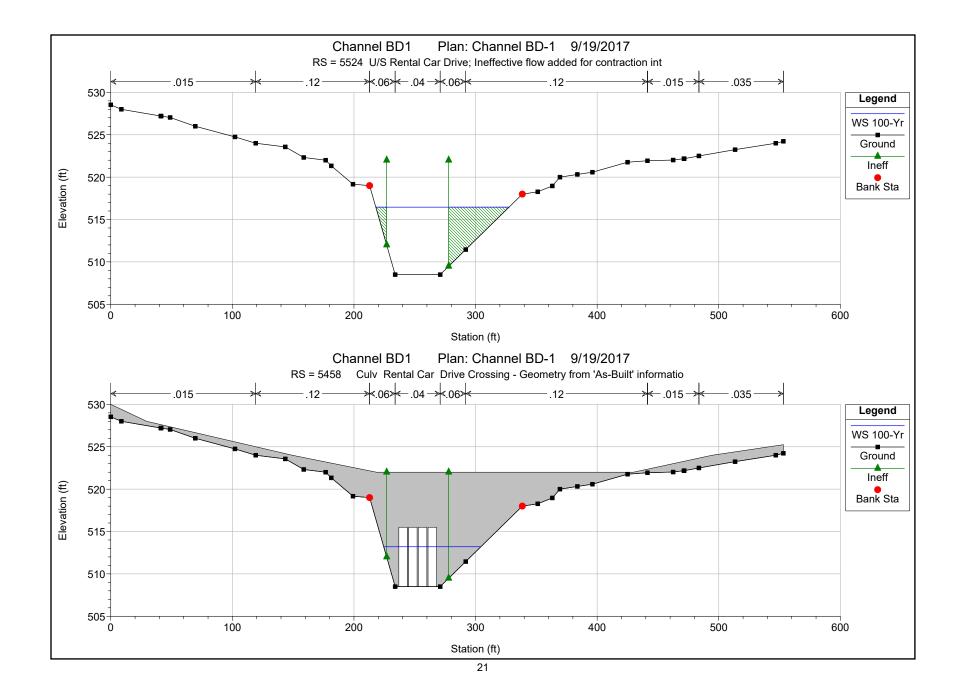


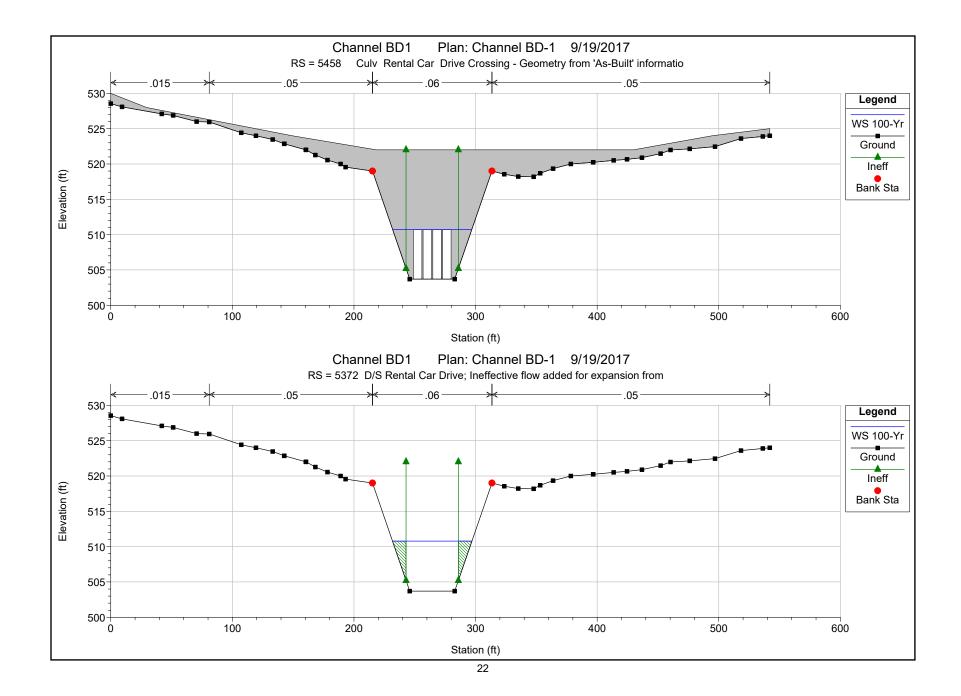


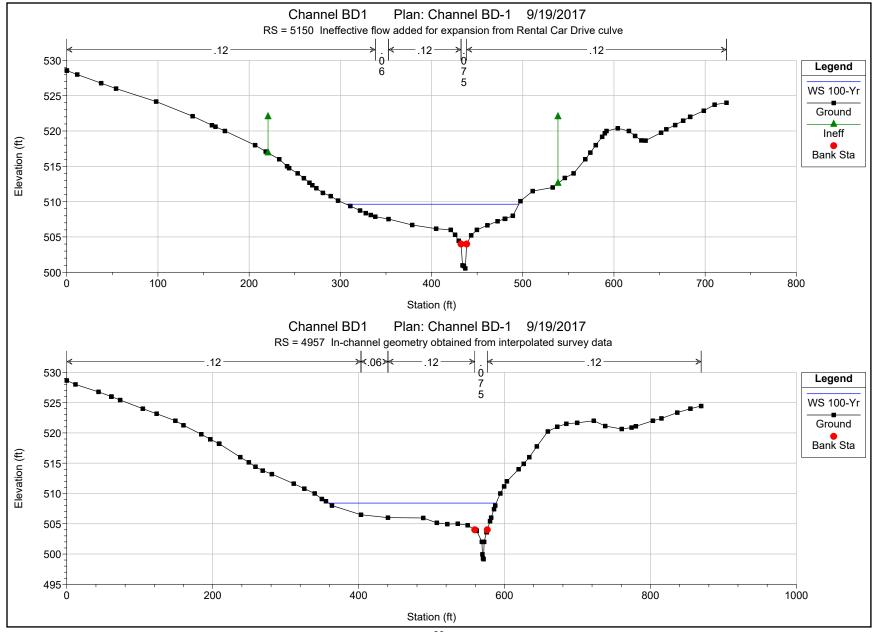


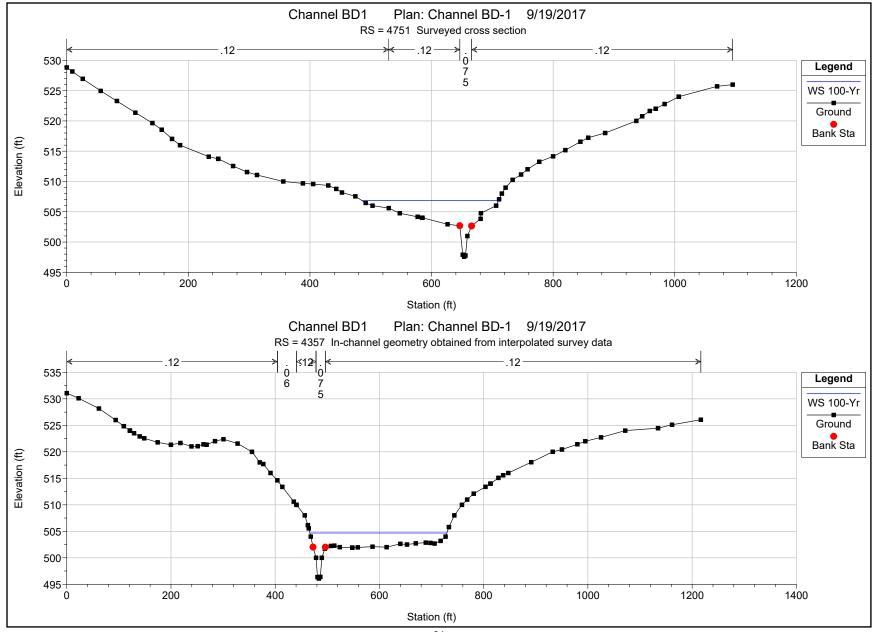


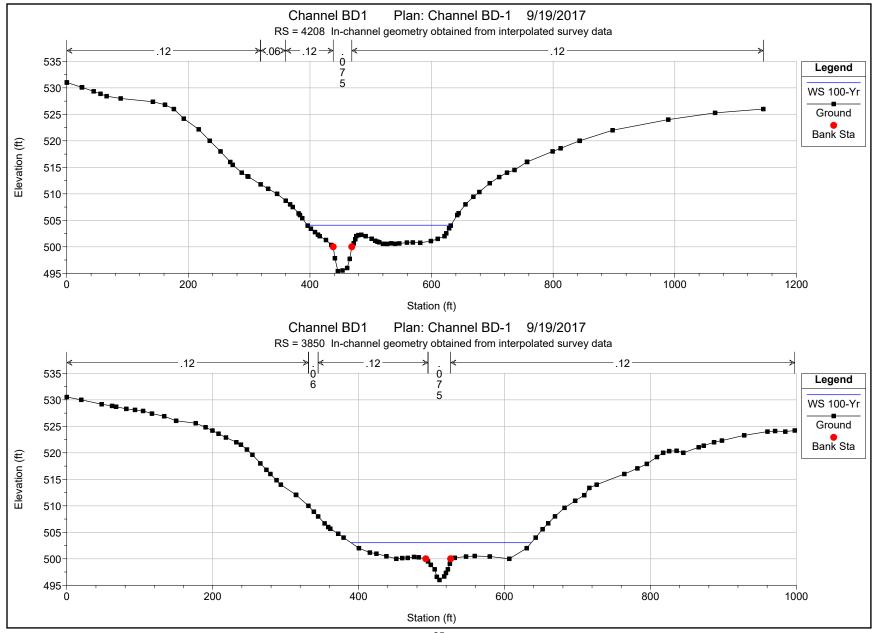


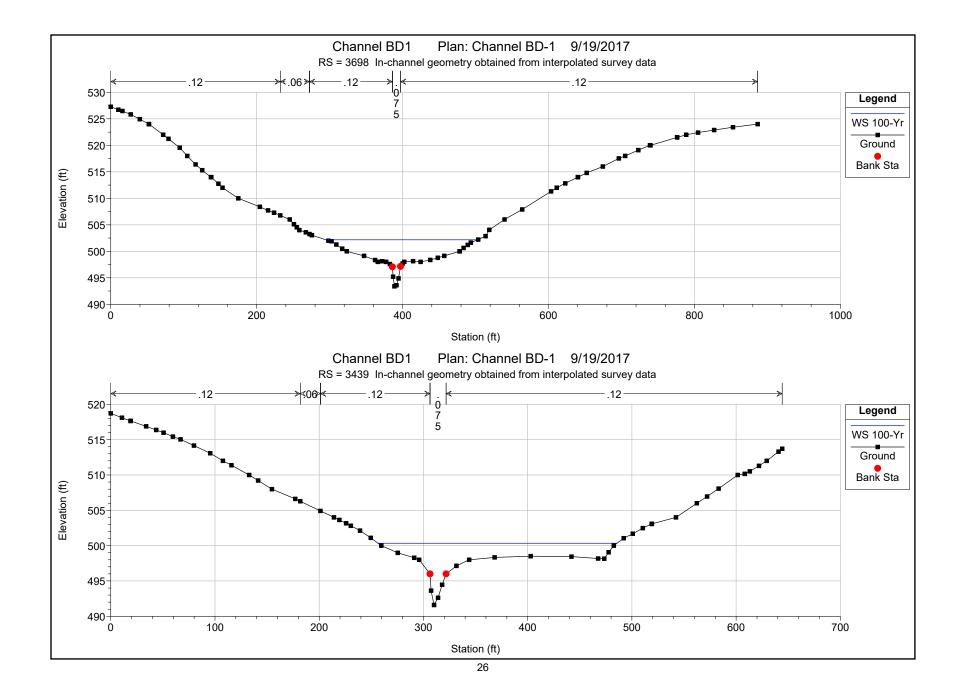


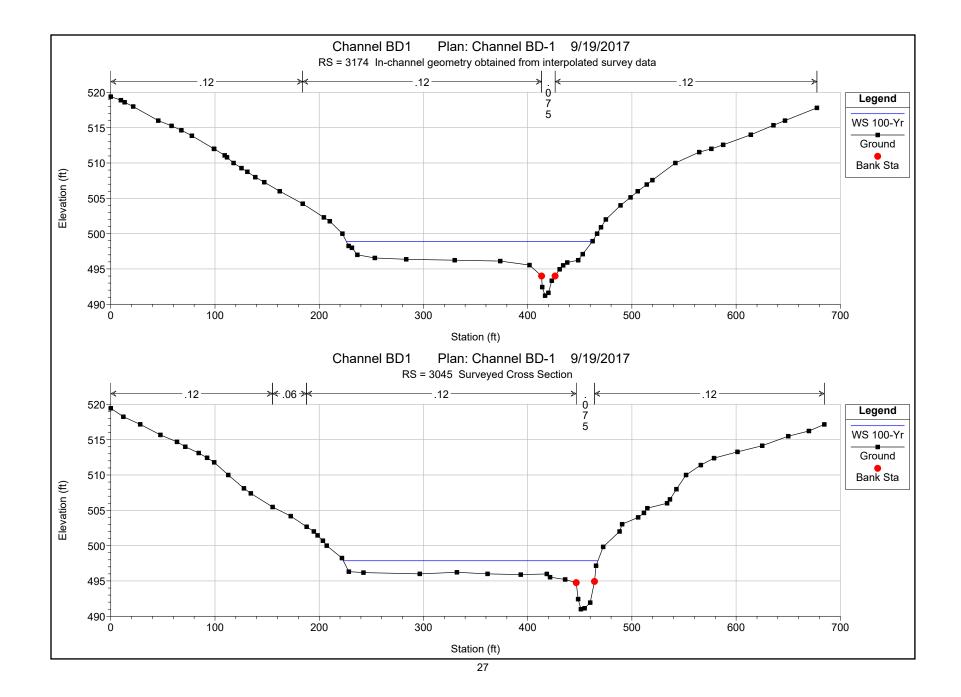


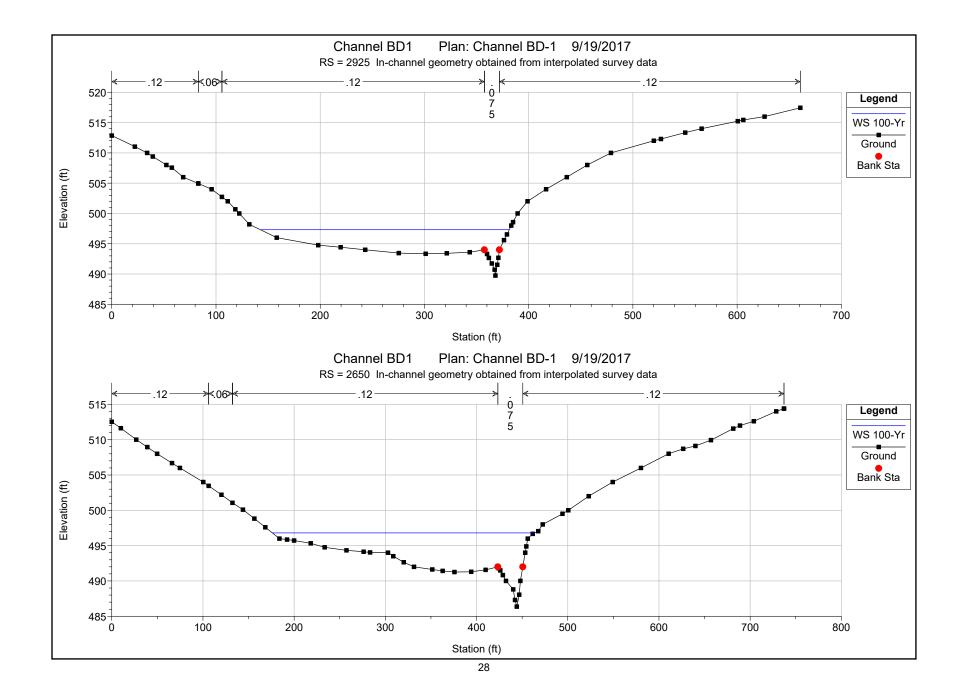


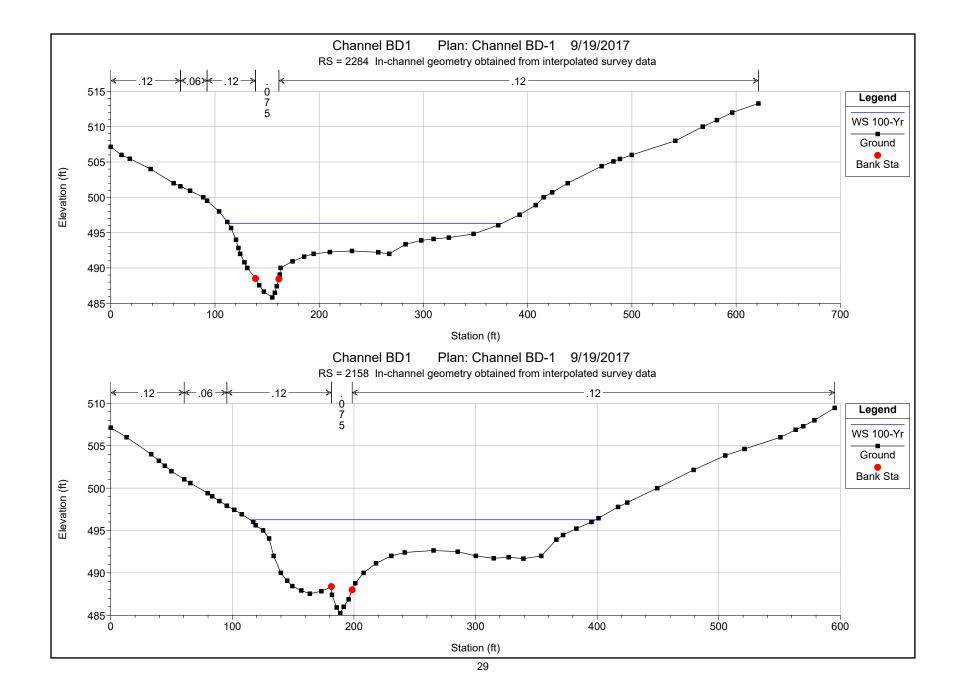


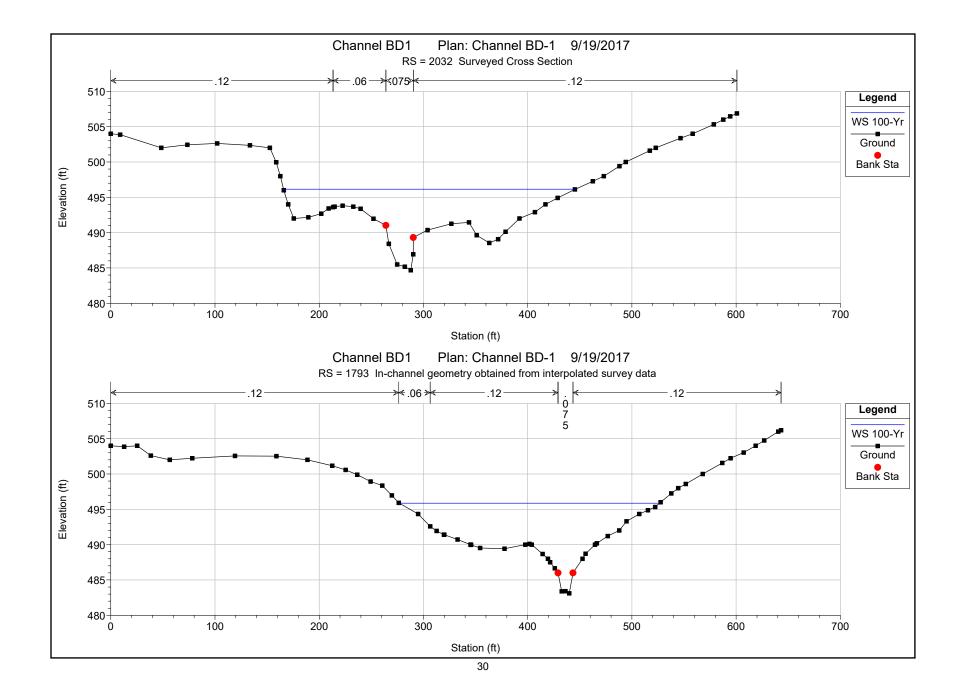


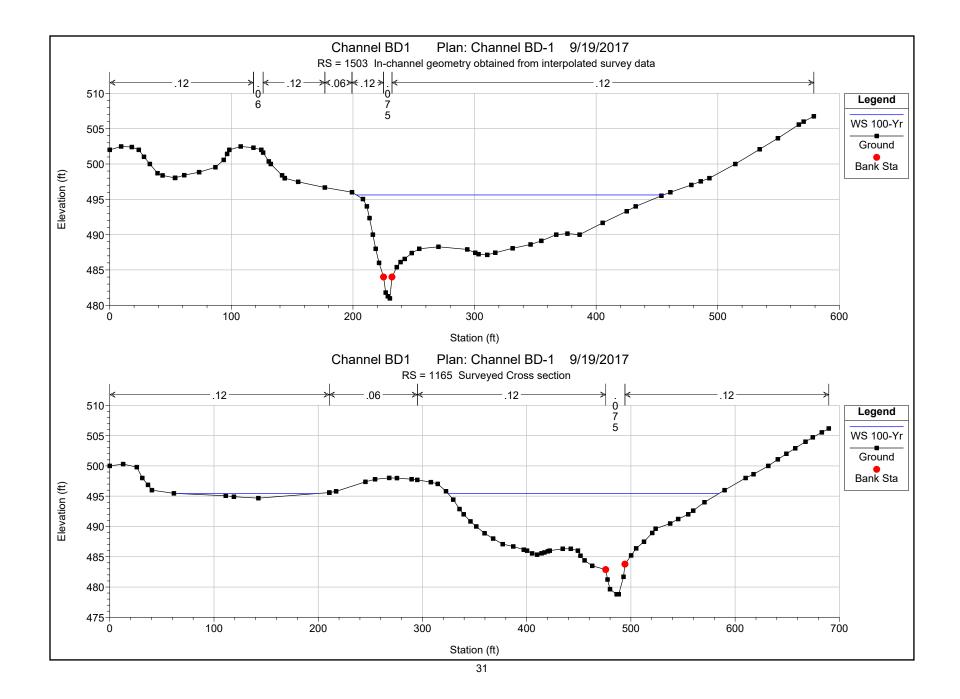


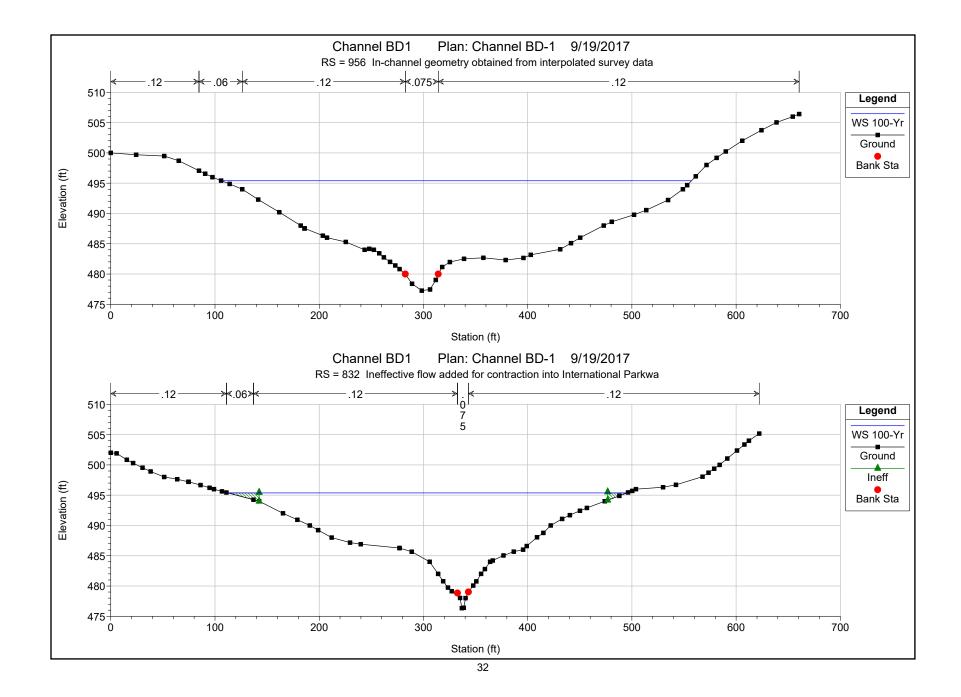


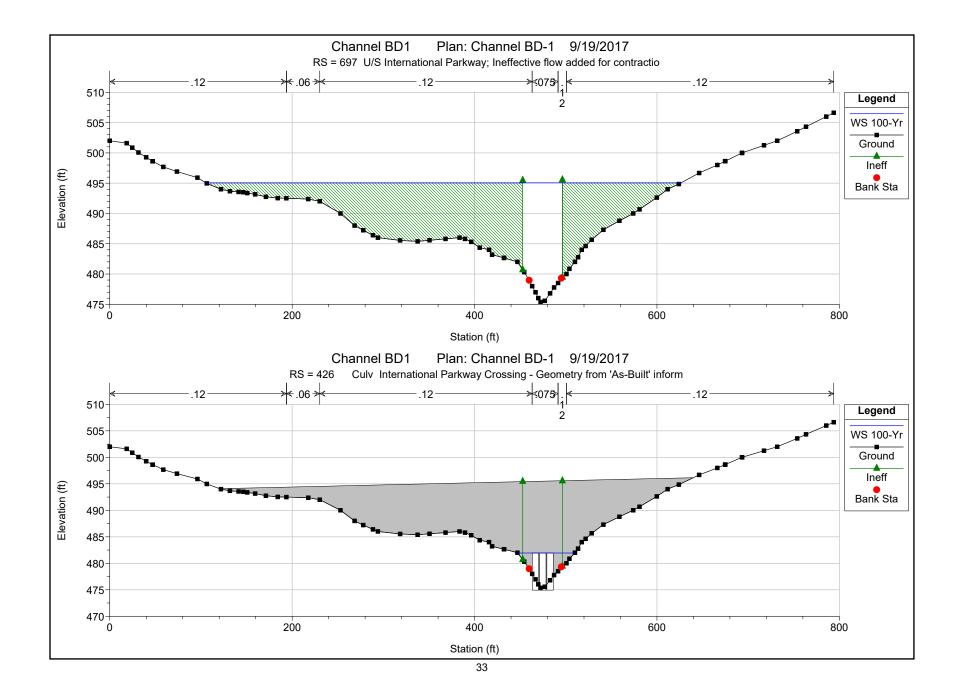


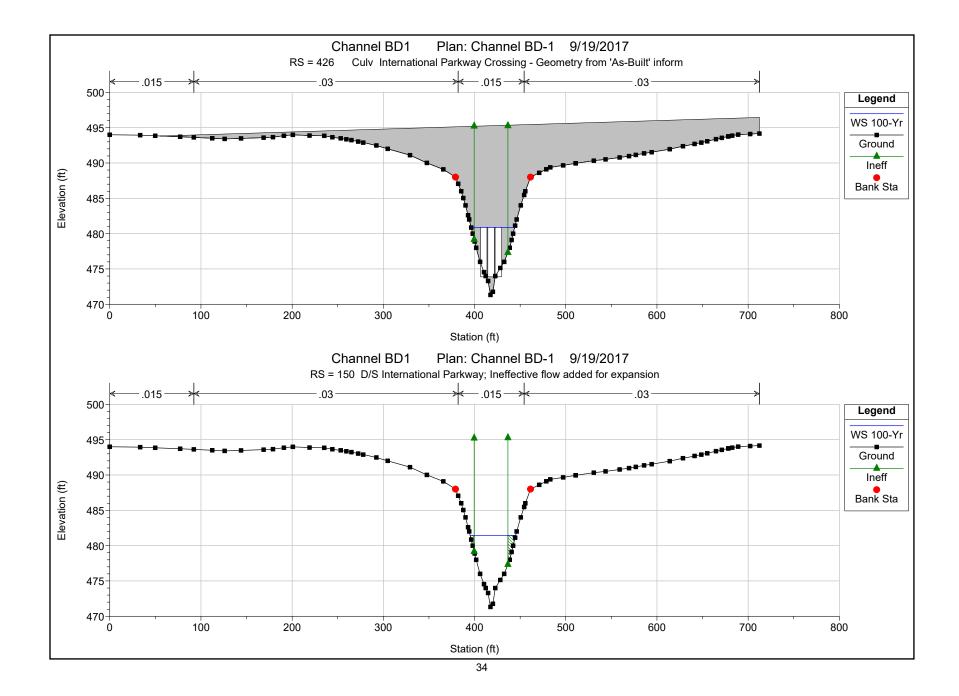


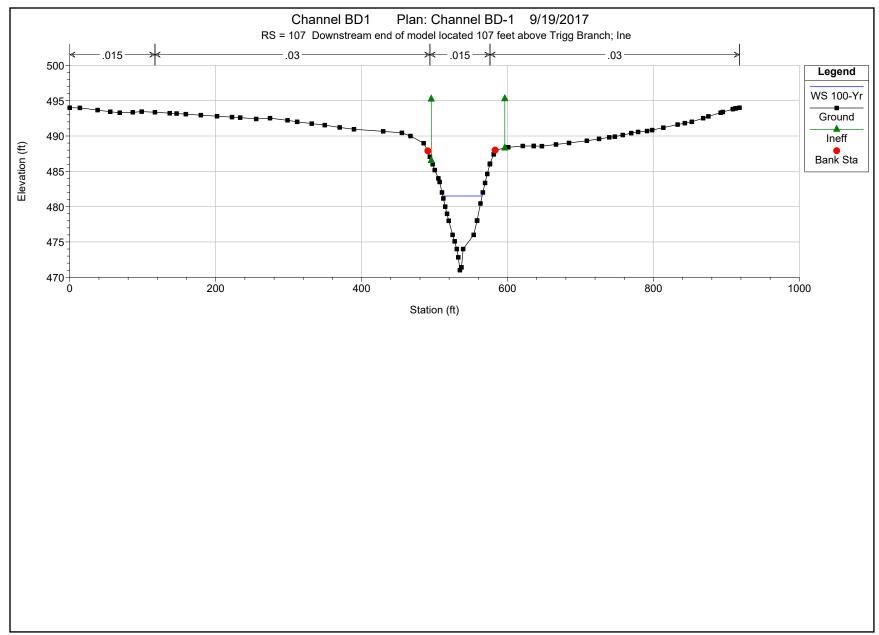


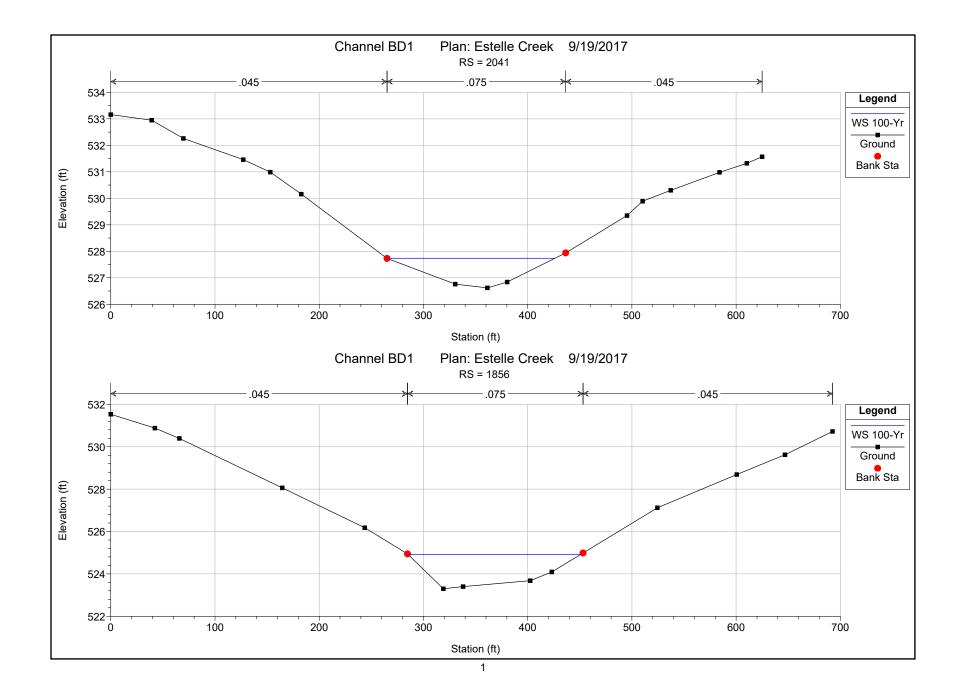


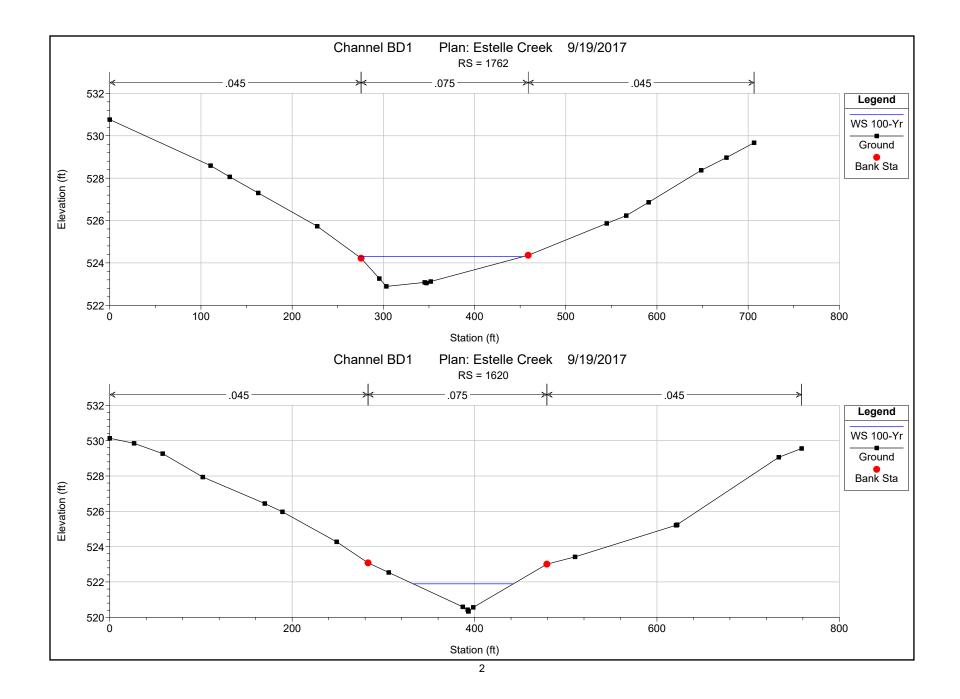


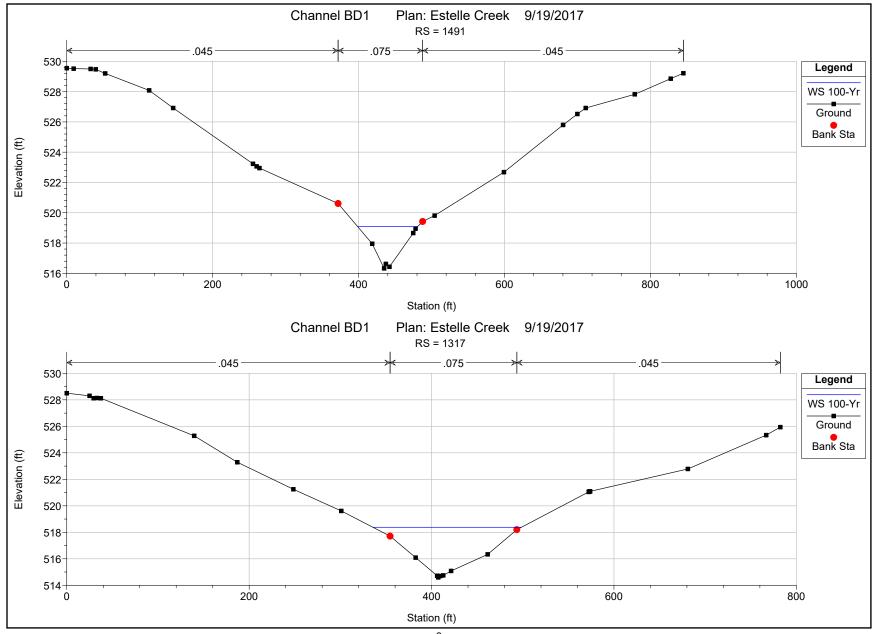


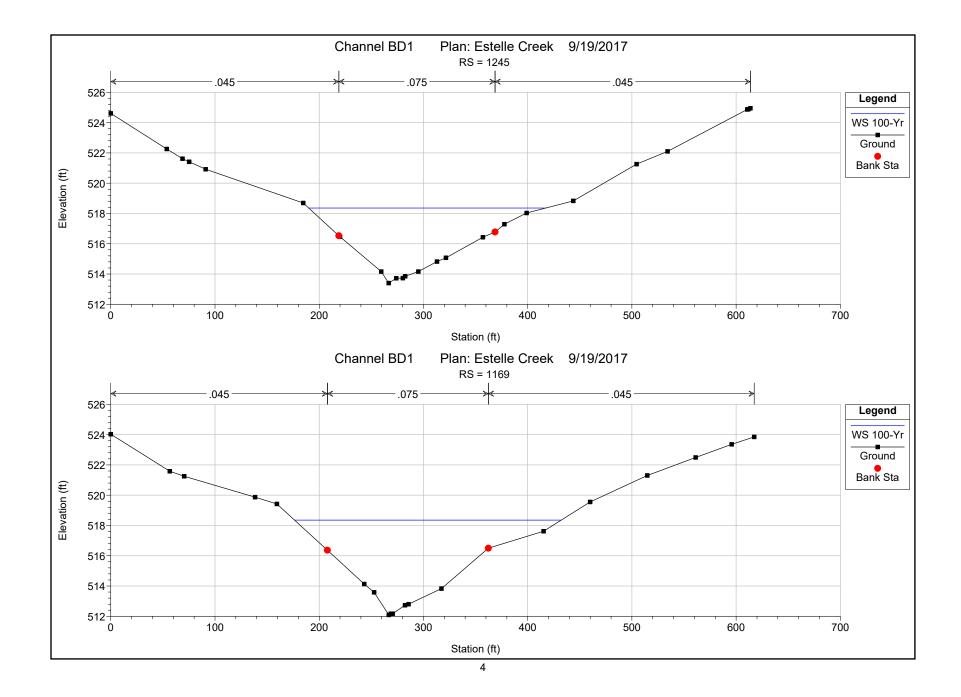


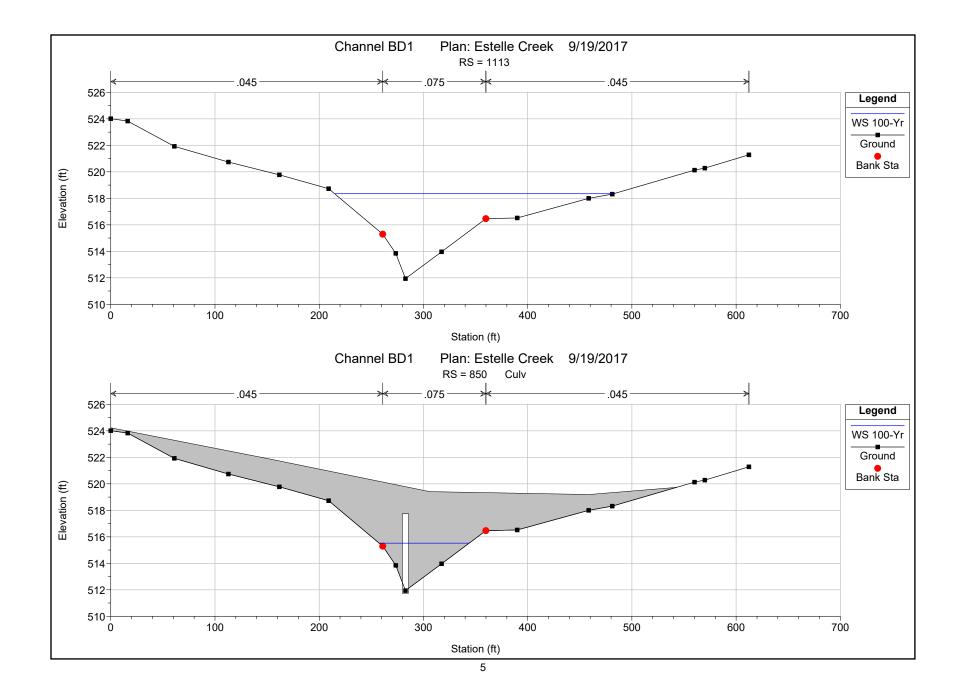


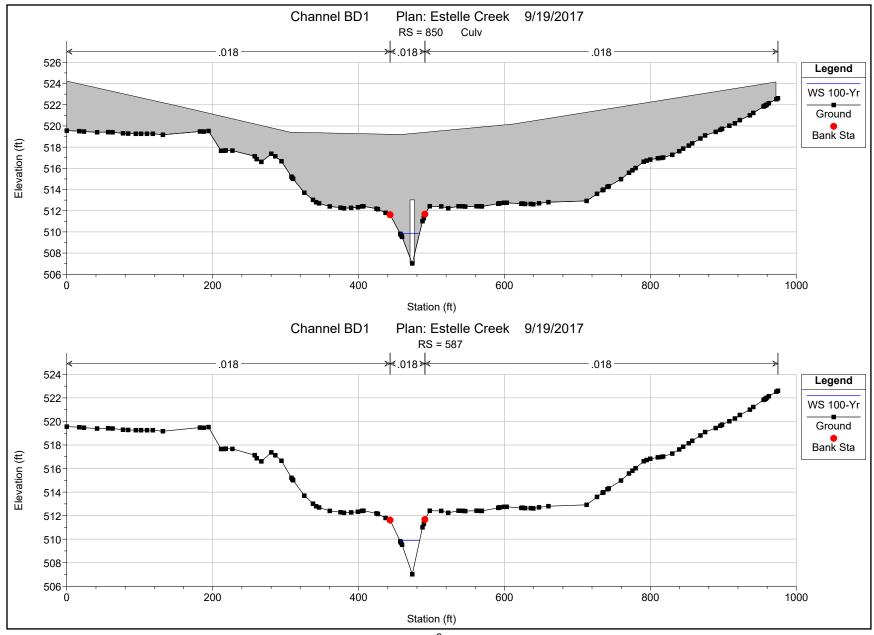


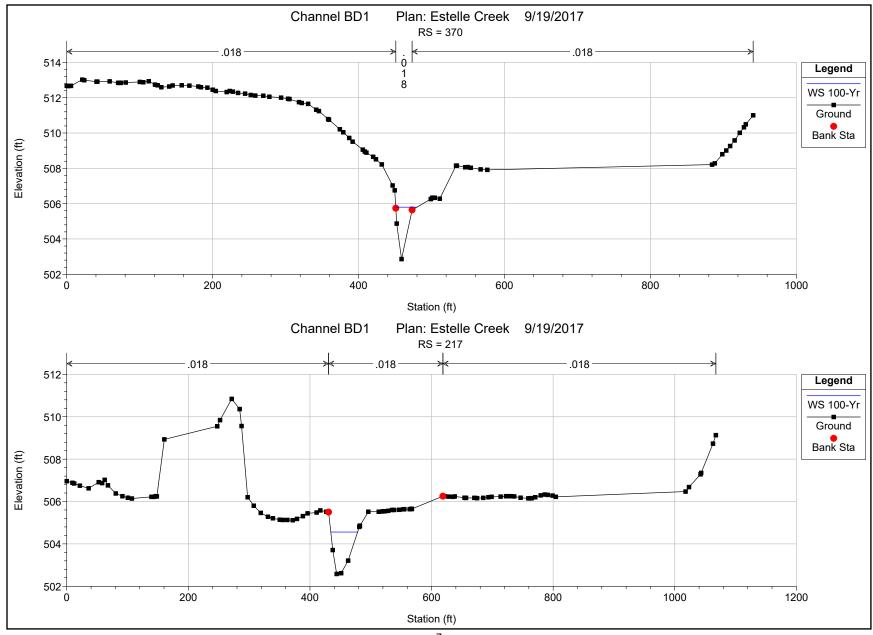


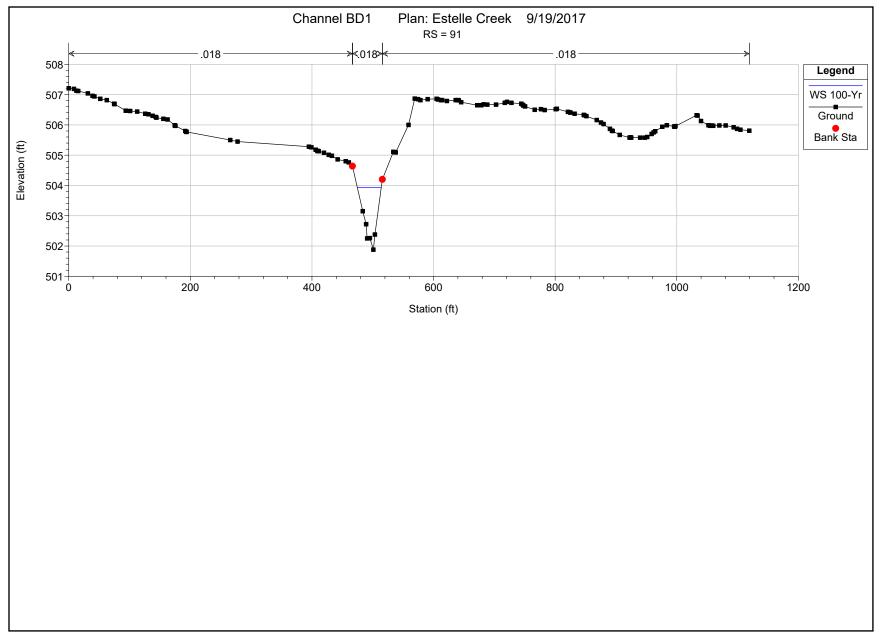




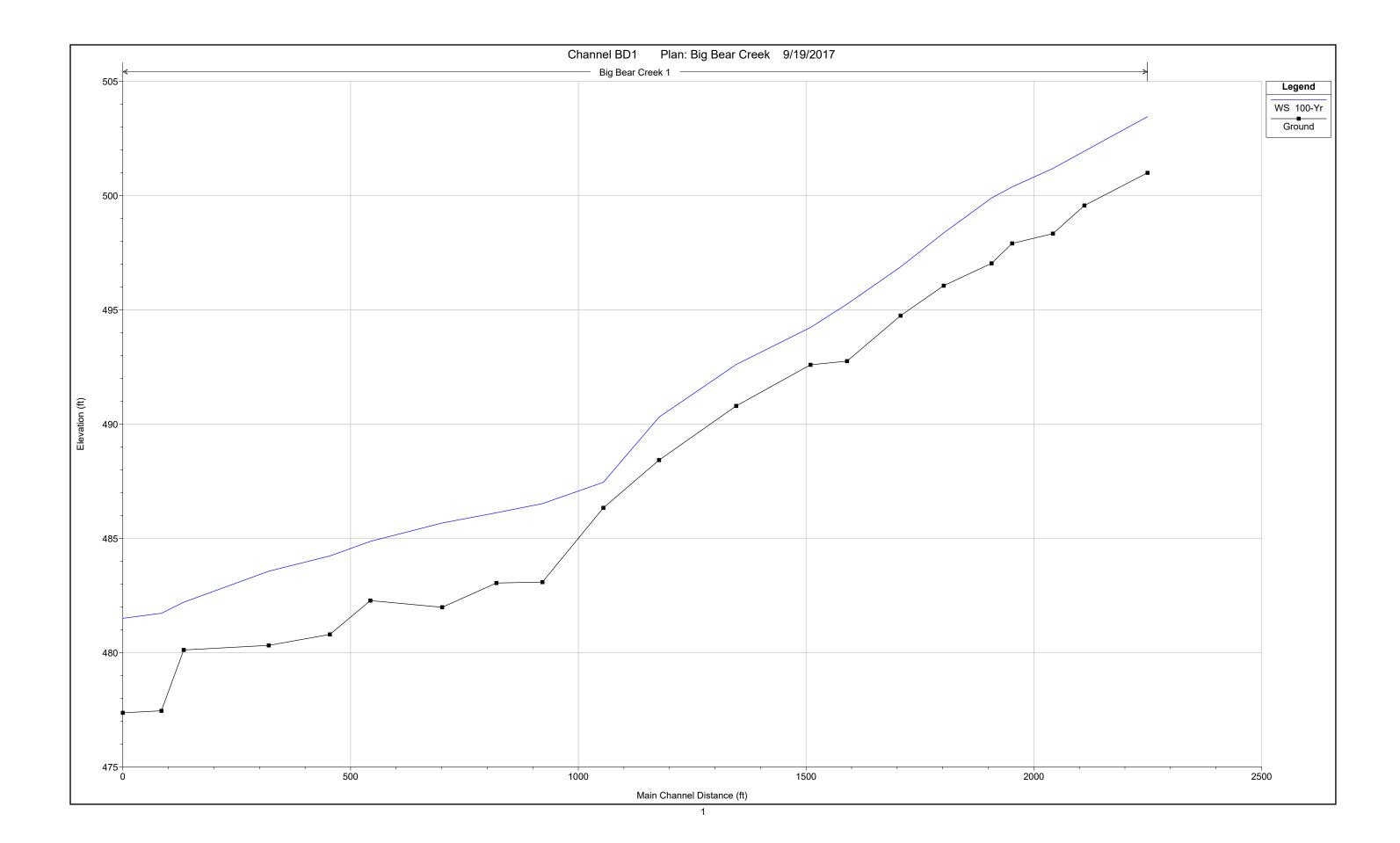


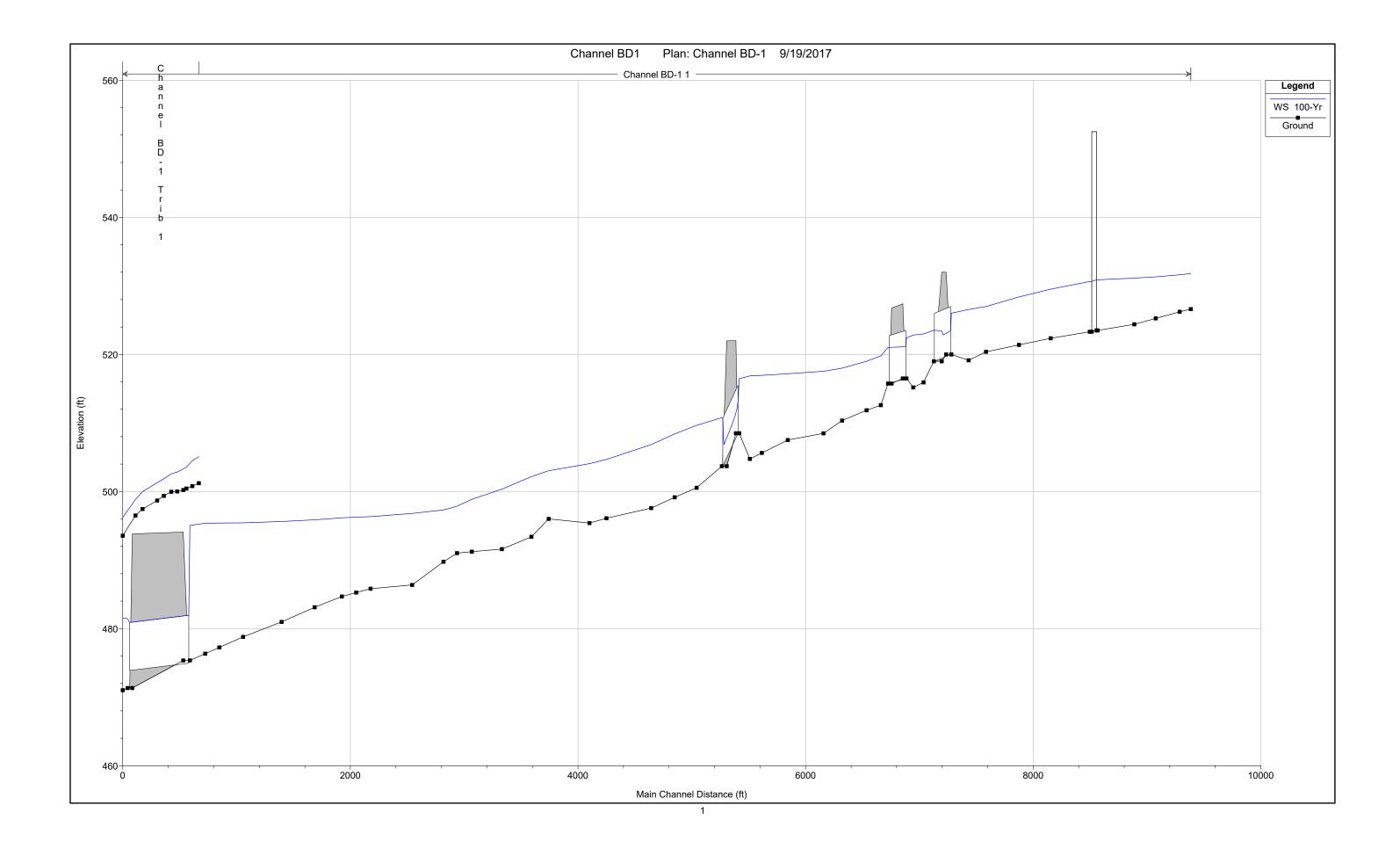


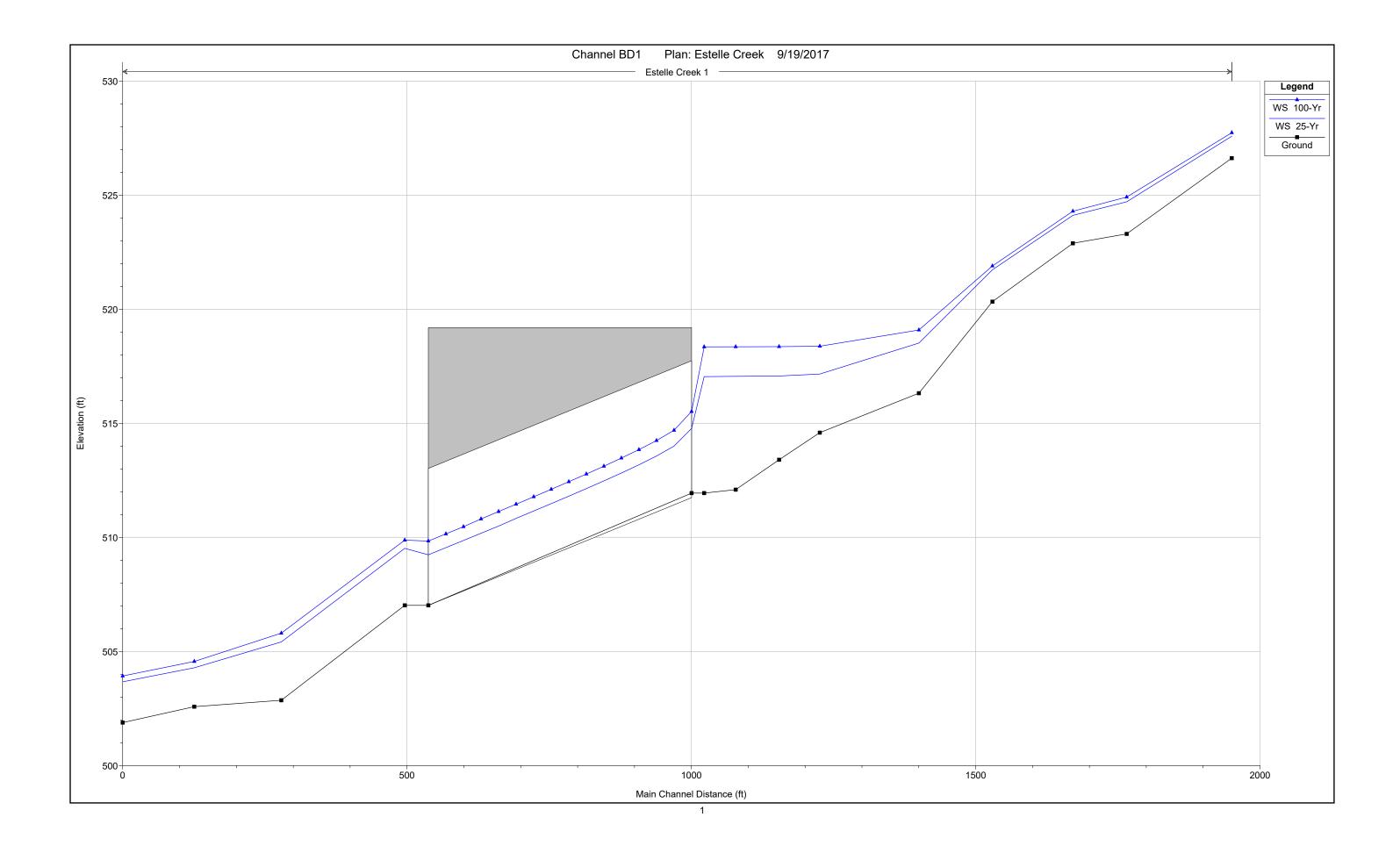




Flood Profile







Existing Conditions Model Output

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
1	2139	100-Yr	320.00	500.99	503.45		503.54	0.008150	2.43	131.52	82.67	0.34
1	2001	100-Yr	320.00	499.56	501.94		502.08	0.014636	3.08	111.97	101.94	0.45
1	1932	100-Yr	320.00	498.33	501.18		501.27	0.008576	2.39	145.45	134.35	0.34
1	1842	100-Yr	320.00	497.90	500.38	499.51	500.49	0.008953	2.88	143.40	138.60	0.37
1	1797	100-Yr	320.00	497.03	499.89		500.03	0.013382	3.68	160.33	188.63	0.45
1	1692	100-Yr	320.00	496.05	498.36		498.47	0.017384	2.60	123.08	123.80	0.46
1	1597	100-Yr	320.00	494.74	496.87		496.96	0.014309	2.40	133.12	130.10	0.42
1	1480	100-Yr	320.00	492.75	495.25		495.32	0.013495	2.19	145.81	156.36	0.40
1	1400	100-Yr	320.00	492.59	494.22		494.29	0.012300	2.05	155.88	172.54	0.38
1	1236	100-Yr	320.00	490.79	492.60		492.65	0.007775	1.87	171.52	155.31	0.31
1	1098	100-Yr	320.00	488.42	490.30	490.04	490.40	0.033257	2.99	147.79	260.05	0.61
1	976	100-Yr	320.00	486.33	487.45		487.52	0.014035	1.75	146.27	165.58	0.38
1	842	100-Yr	320.00	483.08	486.52		486.53	0.003290	1.55	365.63	334.46	0.22
1	778	100-Yr	320.00	483.04	486.11		486.14	0.004638	1.89	320.41	358.71	0.26
1	714	100-Yr	320.00	481.98	485.67		485.70	0.003181	1.68	330.56	388.36	0.22
1	558	100-Yr	320.00	482.27	484.86		484.95	0.008651	2.65	202.31	364.13	0.35
1	469	100-Yr	320.00	480.79	484.23	483.18	484.32	0.006509	2.57	172.15	200.61	0.32
1	335	100-Yr	480.00	480.31	483.56		483.62	0.004151	2.05	254.15	205.16	0.25
1	148	100-Yr	480.00	480.11	482.20		482.37	0.017708	3.32	144.66	102.29	0.49
1	99	100-Yr	480.00	477.45	481.72		481.79	0.004882	2.15	225.26	130.22	0.27
1	14	100-Yr	480.00	477.36	481.50	479.11	481.53	0.001001	1.38	370.50	276.63	0.13

HEC-RAS Plan: BBC ECM River: Big Bear Creek Reach: 1 Profile: 100-Yr

HEC-RAS Plan: CBD1 ECM Profile: 100-Yr

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
1	9492	100-Yr	490.00	526.61	531.79		532.00	0.004463	4.04	151.07	62.60	0.34
1	9394	100-Yr	490.00	526.22	531.62		531.68	0.001156	2.03	241.38	62.96	0.18
1	9184	100-Yr	490.00	525.26	531.32		531.40	0.001595	2.28	215.36	60.36	0.21
1	8996	100-Yr	490.00	524.40	531.13		531.17	0.000629	1.62	303.09	70.40	0.14
1	8674	100-Yr	490.00	523.51	530.89	526.55	530.94	0.000853	1.78	275.92	69.73	0.16
1	8639		Bridge									
1	8604	100-Yr	1080.00	523.31	530.64	527.72	530.90	0.004526	4.08	264.56	66.88	0.36
1	8261	100-Yr	1080.00	522.36	529.53		529.69	0.002254	3.21	336.79	72.85	0.26
1	7982	100-Yr	1080.00	521.39	528.39		528.72	0.006758	4.66	231.93	65.53	0.44
1	7692	100-Yr	1080.00	520.38	526.99		527.20	0.003540	3.70	292.12	72.02	0.32
1	7540	100-Yr	1080.00	519.14	526.56	524.15	526.72	0.002549	3.28	350.70	100.97	0.28
1	7388	100-Yr	1080.00	520.00	526.01	522.68	526.27	0.002530	4.10	263.45	88.61	0.30
1	7318		Culvert									
1	7234	100-Yr	1080.00	519.00	523.53	522.01	524.18	0.009321	6.49	166.31	65.65	0.54
1	7143	100-Yr	1080.00	515.92	522.99	520.52	523.24	0.004284	4.08	268.28	74.41	0.36
1	7053	100-Yr	1080.00	515.19	522.83		522.95	0.001272	2.89	399.00	88.02	0.2
1	6993	100-Yr	1080.00	516.50	522.42	519.36	522.75	0.001447	4.62	233.67	87.69	0.33
1	6904		Culvert									
1	6832	100-Yr	1080.00	515.75	521.03	518.53	521.41	0.004427	4.99	216.29	76.15	0.38
1	6768	100-Yr	1520.00	512.60	519.79	518.82	520.65	0.020246	9.48	279.83	79.34	0.65
1	6643	100-Yr	1520.00	511.85	519.00	516.64	519.23	0.004966	4.77	544.34	154.42	0.3
1	6428	100-Yr	1520.00	510.35	518.00		518.27	0.006564	5.28	521.97	173.49	0.37
1	6264	100-Yr	1520.00	508.49	517.55		517.60	0.001149	2.40	1180.15	346.44	0.16
1	5951	100-Yr	1620.00	507.51	517.19	513.40	517.28	0.001732	2.94	911.41	220.73	0.19
1	5723	100-Yr	1620.00	505.62	516.95		517.00	0.000985	2.64	1290.76	283.81	0.15
1	5618	100-Yr	1620.00	504.75	516.87	509.13	516.91	0.000322	1.60	1278.06	243.66	0.09
1	5524	100-Yr	1620.00	508.50	516.46	511.96	516.72	0.001131	4.15	390.04	109.51	0.26
1	5458		Culvert									
1	5372	100-Yr	1730.00	503.70	510.78	507.49	511.29	0.004167	5.77	299.79	65.31	0.39
1	5150	100-Yr	1730.00	500.55	509.64	508.57	509.88	0.013125	6.47	524.24	189.35	0.40
1	4957	100-Yr	1730.00	499.15	508.41		508.58	0.008264	4.96	609.25	229.93	0.30
1	4751	100-Yr	1730.00	497.58	506.84		507.10	0.008053	5.68	603.28	224.66	0.39
1	4357	100-Yr	1730.00	496.09	504.68		504.84	0.009406	4.68	671.34	262.79	0.3
1	4208	100-Yr	1730.00	495.40	504.07		504.24	0.003396	4.20	779.54	236.17	0.2
	3850	100-Yr	1730.00	496.00	503.03		503.22	0.006676	4.73	676.40	247.03	0.3
1	3698	100-Yr	1730.00	493.39	502.17		502.37	0.008268	5.89	635.93	207.98	0.3
1	3439	100-Yr	1730.00	491.60	500.34		500.75	0.013280	7.28	531.49	229.25	0.49
1	3174	100-Yr	1730.00	491.23	498.87		499.07	0.008535	5.79	661.46	235.80	0.40

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
1	3045	100-Yr	1730.00	491.01	497.86		498.26	0.015984	7.33	521.32	244.25	0.54
1	2925	100-Yr	1730.00	489.75	497.31		497.42	0.006868	4.34	737.36	238.73	0.34
1	2650	100-Yr	1730.00	486.37	496.81		496.88	0.002146	3.18	1055.54	287.80	0.21
1	2284	100-Yr	1730.00	485.82	496.33		496.44	0.001817	3.68	1018.32	263.08	0.21
1	2158	100-Yr	1730.00	485.25	496.26		496.31	0.001047	2.80	1329.01	284.24	0.16
1	2032	100-Yr	1730.00	484.68	496.15		496.20	0.000879	2.42	1288.38	280.02	0.14
1	1793	100-Yr	2520.00	483.11	495.87		495.97	0.001855	4.10	1291.18	249.72	0.21
1	1503	100-Yr	2520.00	480.97	495.62		495.67	0.001461	3.41	1532.22	252.67	0.16
1	1165	100-Yr	2520.00	478.79	495.43		495.47	0.000534	2.54	2012.35	391.55	0.11
1	956	100-Yr	2520.00	477.25	495.40		495.41	0.000092	1.25	4141.54	450.89	0.05
1	832	100-Yr	2520.00	476.34	495.37	485.66	495.39	0.000309	2.15	2688.18	382.51	0.09
1	697	100-Yr	2520.00	475.35	495.05	482.44	495.23	0.000893	3.53	759.09	520.85	0.15
1	426		Culvert									
1	150	100-Yr	2520.00	471.33	481.46	480.19	483.16	0.001020	10.46	240.91	49.95	0.72
1	107	100-Yr	2520.00	471.01	481.51	480.11	482.74	0.001000	8.91	282.76	53.94	0.69
Trib 1	829	100-Yr	380.00	501.21	505.09		505.30	0.012628	3.89	127.96	88.39	0.45
Trib 1	772	100-Yr	380.00	500.79	504.49		504.56	0.010550	2.91	201.70	154.93	0.37
Trib 1	720	100-Yr	380.00	500.43	503.57	503.14	503.81	0.019148	4.30	118.96	171.51	0.54
Trib 1	693	100-Yr	380.00	500.22	503.30	502.54	503.38	0.010641	2.35	161.66	131.36	0.37
Trib 1	639	100-Yr	380.00	500.00	502.84		502.93	0.006326	2.41	163.36	117.44	0.31
Trib 1	587	100-Yr	380.00	499.96	502.58	501.27	502.64	0.004536	1.94	196.38	150.45	0.26
Trib 1	521	100-Yr	380.00	499.37	501.86		502.13	0.019918	4.18	91.01	49.10	0.54
Trib 1	463	100-Yr	380.00	498.69	501.29	499.97	501.35	0.004637	2.03	187.34	118.69	0.26
Trib 1	334	100-Yr	380.00	497.44	499.99		500.30	0.028087	4.46	85.11	54.13	0.63
Trib 1	272	100-Yr	380.00	496.51	498.84		498.98	0.012869	3.01	126.12	81.02	0.43
Trib 1	160	100-Yr	380.00	493.55	496.21	495.97	496.69	0.046702	5.57	68.28	46.91	0.80

HEC-RAS Plan: CBD1 ECM Profile: 100-Yr (Continued)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
1	2041	100-Yr	250.00	526.62	527.74	527.45	527.83	0.026503	2.41	103.83	161.15	0.53
1	1856	100-Yr	250.00	523.30	524.91		524.94	0.004566	1.41	177.91	165.38	0.24
1	1762	100-Yr	250.00	522.89	524.29		524.34	0.010422	1.75	142.96	179.90	0.34
1	1620	100-Yr	250.00	520.33	521.89	521.65	522.04	0.036192	3.08	81.18	109.88	0.63
1	1491	100-Yr	250.00	516.32	519.09		519.16	0.008099	2.20	113.39	82.22	0.33
1	1317	100-Yr	250.00	514.59	518.38		518.39	0.000566	0.80	315.44	162.67	0.09
1	1245	100-Yr	250.00	513.40	518.36		518.36	0.000115	0.47	552.39	227.45	0.05
1	1169	100-Yr	250.00	512.09	518.35		518.35	0.000046	0.35	750.52	255.85	0.03
1	1113	100-Yr	250.00	511.94	518.35	513.94	518.35	0.000072	0.44	623.76	267.60	0.04
1	850		Culvert									
1	587	100-Yr	250.00	507.02	509.88	509.88	510.57	0.004385	6.69	37.40	27.01	1.00
1	370	100-Yr	250.00	502.86	505.80	505.80	506.55	0.003954	6.95	36.44	29.08	0.97
1	217	100-Yr	250.00	502.58	504.56		504.89	0.002394	4.61	54.21	44.15	0.73
1	91	100-Yr	250.00	501.88	503.93	503.93	504.47	0.004672	5.90	42.37	39.34	1.00

HEC-RAS Plan: EC ECM River: Estelle Creek Reach: 1 Profile: 100-Yr

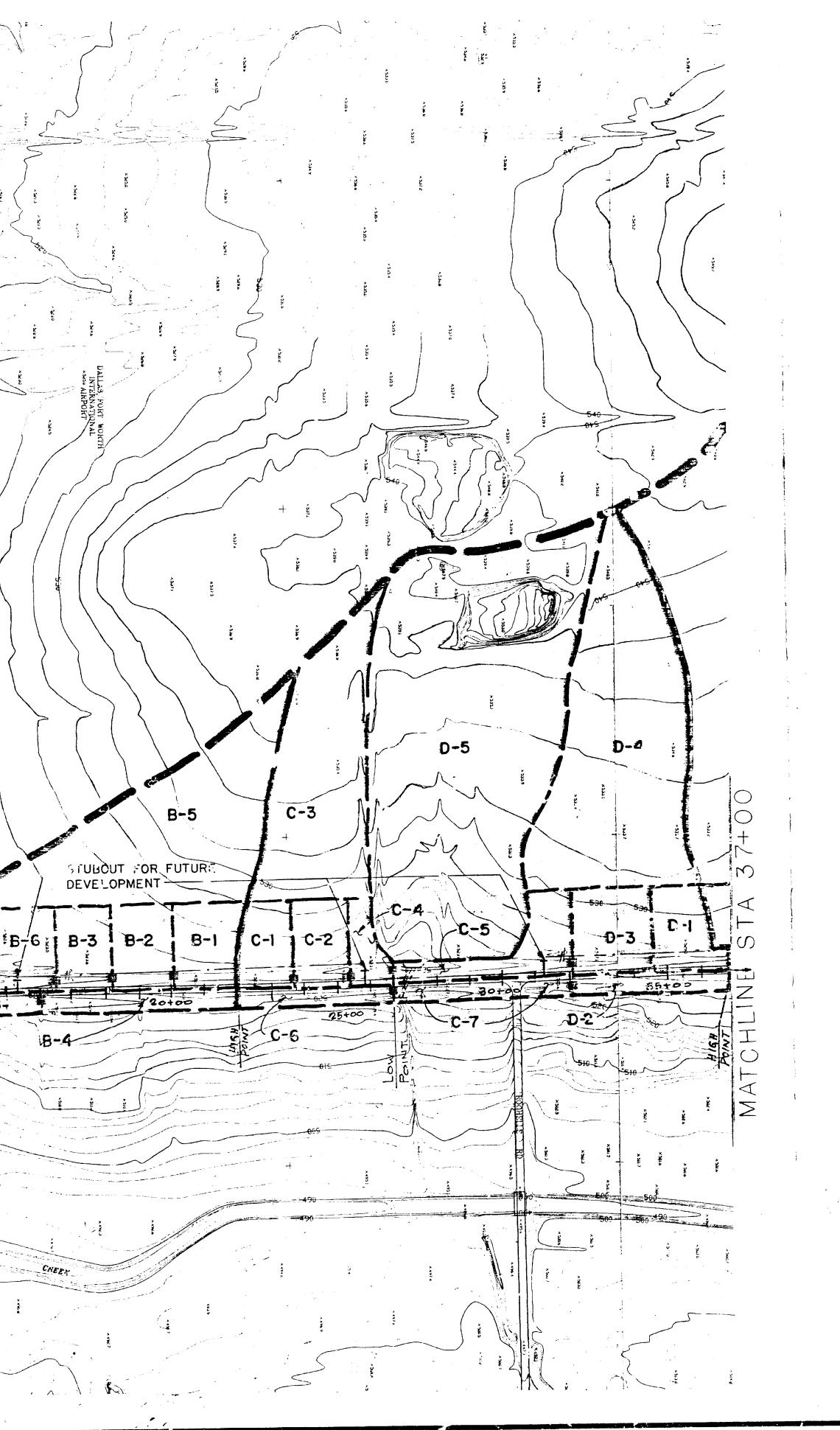
Appendix C

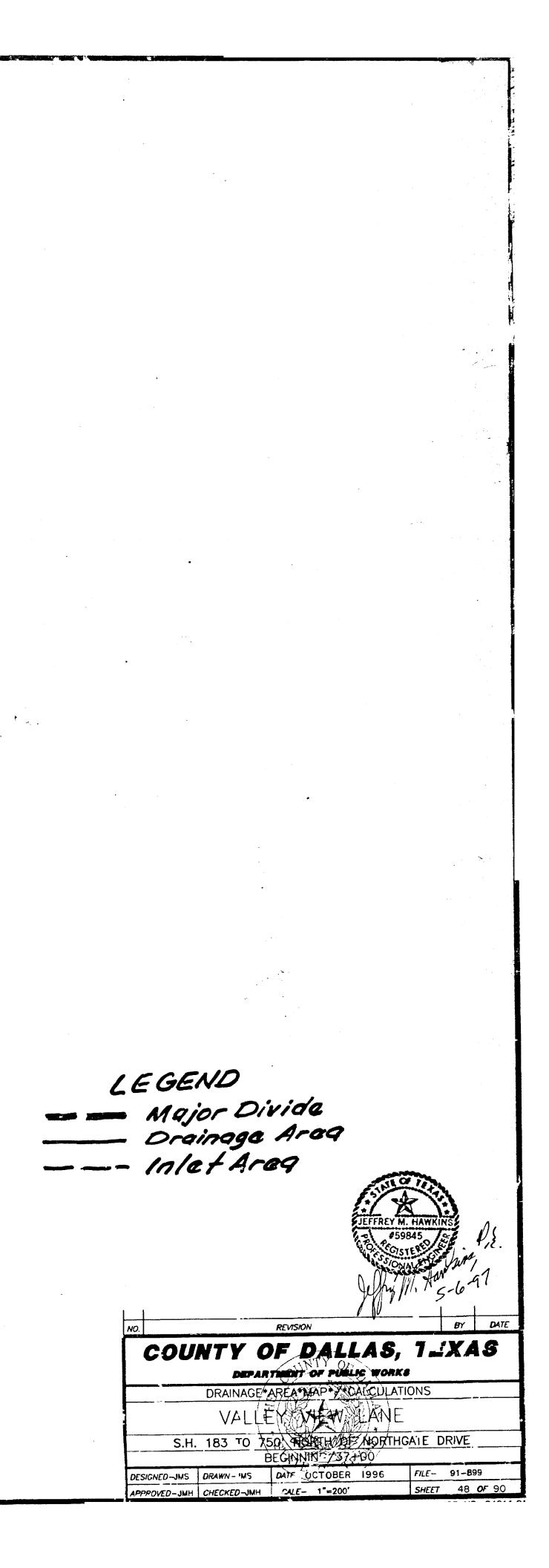
Engineered Plans

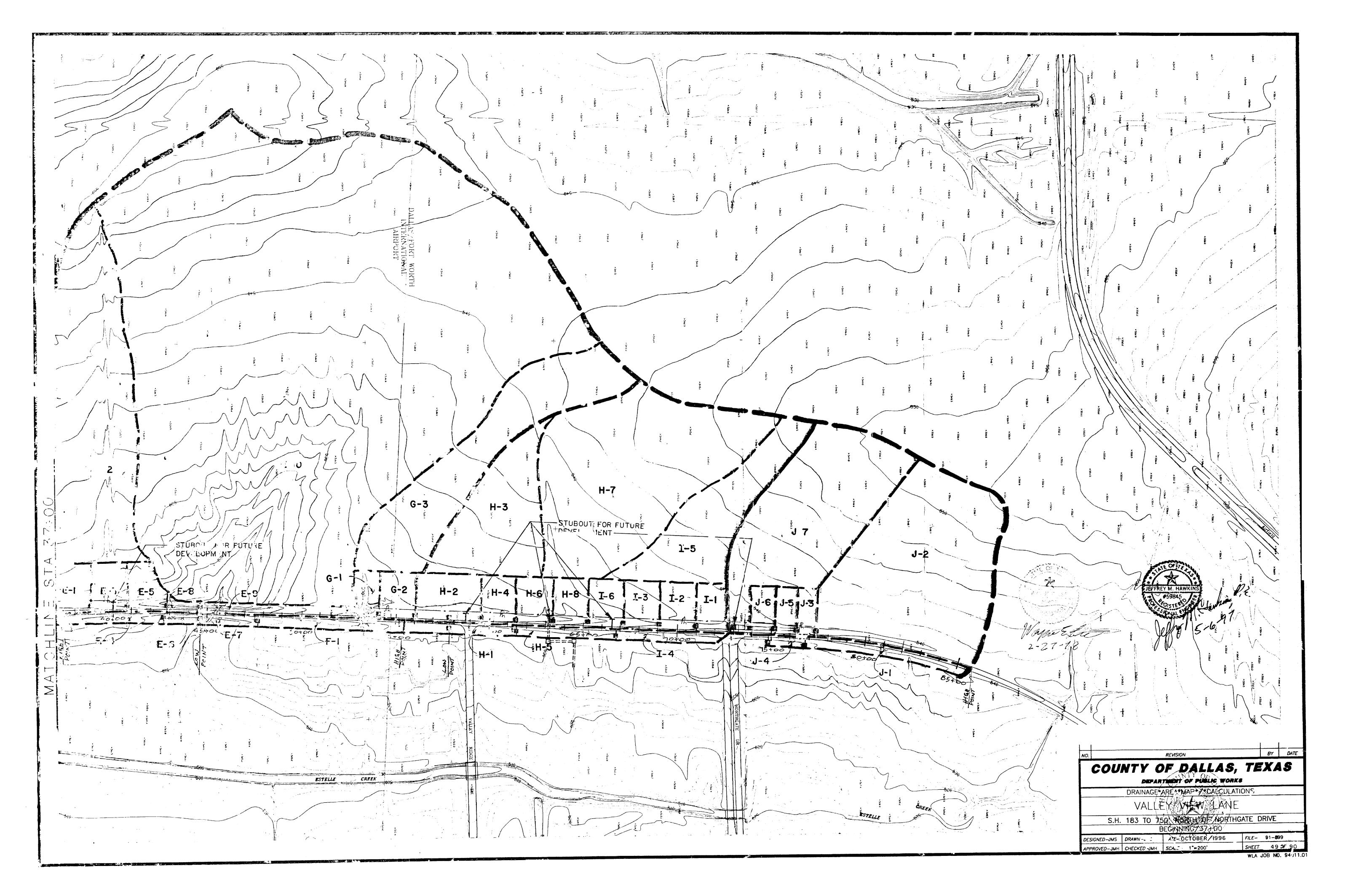
- Valley View Lane
- State Highway 183 (Dallas)
- State Highway 183 (Irving)
- International Parkway

Valley View Lane

42 B-10 1 E 3 _____ 56 ES, ELLE CREEX







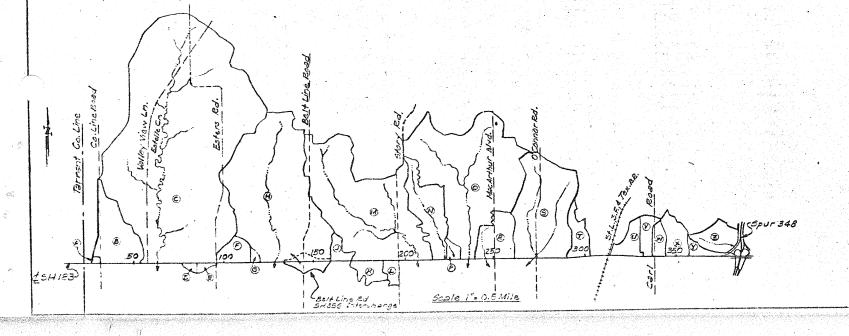
State Highway 183 (Dallas)

RUN-OFF COMPUTATIONS

-													
STATION	DRAINAGE ARE A	AREA (AC)	T	c	1	Q							
31+02	A	3.13	13	0.9	4.4(2)	13							
41+54	В	170.76	29.7	0.58	4.000			=nd 10					and the second sec
63+30	С	1,846.75	98	0.73		3778	Ext.	3-10'×1	р'мэс и	1.5.¢ D.S.	- Add R	extra	barrels
75+00	D.	6.52	12.7	0.90	4.4(2)	26		nd 3'x			· · ·	1	
85+38	E	6.16	30	0.90	5.7 (50)	32	Prop	. 42"	RCP	CO	vert		
112+07	F	55.58	Li I	0.70		222		nd ex	1	ł	1	1	
120+66	G	15.10	U	0.90	'n	78	Ext	end e:	kist. 3'	× 3' . U	S. & D.	5.	
128+57	Н	833.29	47.3	0.70	4.4 (50)	2,567	·Ext.	4.7×6	мас и.	5. ± D.5 -	Add 4	extre b	arrels.
164+80	J	39.54	30	0.70	4.4(10)	122	. Com	plete	CUIVER	t exis	ing (7'×3')	
158+00	к	59.20	16.6	0.50	5.0(5)	98.	To	Storm	Jewe	r 37.	tem	n wange Tang tang tang tang tang tang tang tang t	
196+70	L	25.30	11.1	0.50	5.8(5)	73.		Storn	1 .	1	1	1	
208+37	М	705.84	39.2	0.48	3.75(19)	1.271.	Com	dete d	ulver	t exis	ting (4	6'×6')	
224+00	N	200.00	30	0.50	3.8 (5)	380.	To	Storr	n Sew	er sy	stem		
23/470	P	17.50	n	0.70	3.5(5)	47.	£	Stori	1	1 .	1	1	n na stand A Na standar
235+55	Q ·	249.34	60.8	0.66	2.9 (10)	1,242.	T.	olete		1			
245+30	R	99.85	30	0.70	4.400	308.		plete					
273+16	5	384.39	- 11	0.48	t,	812.	1	olete	1	1			2
299+53	T	49.94		0.52	11	114.	31	end	1				
330+94	U	41.50	н	0.70		128.	11	÷. 3 - 34	4				1
33/+00	. V	Q(U+	()- 6	(U)		127.	11	+.4C"x2	1	1		1	
3 42 +33	W .	25.23	F	0,50	4.400)	56.		plete					icr)
355+55	X	56.23	<i>j</i> 2	0.70	11	173.		end d					· · · ·
372+53	Y	24.29	<i>P</i>	0.90	4	96.		tend e					
587+67	Z	79.96	. N	0.90		316.		and e					
33019	(U+V)	81.90	78	0.70	. 4	255.	Ext	exist.	2-6'×'3'	a.s ci	phiect	to pip	es U.S.
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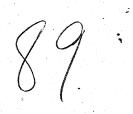
NO		3		OUTLE	r ci	HANNE								CULVE	RT					• .		
STATION	Q	ALLOW	w	SS	n	s	тw	SIZE, LENGTH, & DESCRIPTIO	N d _c	Sc	s	<u>v²</u> 29	Ce	he	hf	Ĥ	Р	SL	нw	Vout.	TYPE OPER.	REMARKS
31+02	13		4	3:1	0.02	1.8	0.72				Ī											storm sewer
41+54	435		10	35:1						1			··· • · · · · · ·									Storn Sewer
63+30	3,778	11.00	30	4:1	0:025	0.38%	6.20	5-10'×10 × 285.5' MBC	5.6	0.31	0.405			· · · · · · · · · · · ·					9.5	14.85	111	Add 2-10'x10' barrets
75+00			4	3:1	0.025	2.0%	1.00											• *				Storm Sewer
35+38	32	3.0	6	16:1	0.025	1.85%	1.46	42"×275' RCP Culv.	2.84	0.58	0.65		2 - 11 - 1 2 - 1		· · · · · · · · · · · · · · · · · · ·				2.45	10.0	III	
112+07	222	6.0	6	8:1	0.025	3.32%	1.72	GxGx304 BoxCulv.	3.5	0.39	0.366	1.74		0.61	0.73			0.58	6.00	9.48		مراجع میں معاملہ میں ایک اور ایک اور ایک اور ایک ایک ایک ایک ای ایک ایک ایک ایک ایک ایک ایک ایک ایک ایک
120+66	2	4.5	4	8:1	0.035	4.76%	0.8	3'x 3'x 306' Box Culv.	2.8	0.58	2.048					2.6	2.9			8.66		an a
128+57	2.567	7.0	20	10:1	0.025	3.62%	5.05	8-7×6'×275' MBC	4.0	0.25	0.578	a patrica della			nan i Guarda				6.98		<u>II</u>	Add 4-7×6 barrels
299+5	114.	4.6	4	10:1	0.035	0.75%	1.78	6'x 2'x 224.75' Box Culy.	2.2	0.34	0.45		• • • •			2.85		0.12	1	9.6	IV	المی میکند. با این این این این این این این این این ای
330+94	128	4.0		<u> </u>	-	-	3.0	3-36" RCP (existing)	2.1	0.47	0.3	· · · · · · · · · · ·			· · · · · · · · · · · · · · · ·	1.0				6.2	1	Disch. into junct. box
330+94	255	-	-	-	-	-	-	2-6×3'× 187'MBC	2.4	0.15						4.26	2.70	3.68	3.28	17.8	\overline{M}	Continues off R.D.W.
355+55	173	4.0	10	4:1	0.025	0.86%	2.2	2-6'x3'x 258'MBC	1.9	0.32	0.474								1	8.9	1	A second seco
372+52	96	4.0	4	6:1	0.035	0.36%	1.41	6'x2'x 255'.30x Culv.	2.0	0.33	0.33					2.10	2.0	0.36	3.74	8.0	至	
587+67	316	5.0	-	-	-	-	-	3-60"×520.7 R.C.P.	2.9	0.35	5 0.7						- · ·		4.5	11.8	\square	Disch into exist. pipes
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* W. B. Frt. Rd Stationing



CULVERT COMPUTATIONS



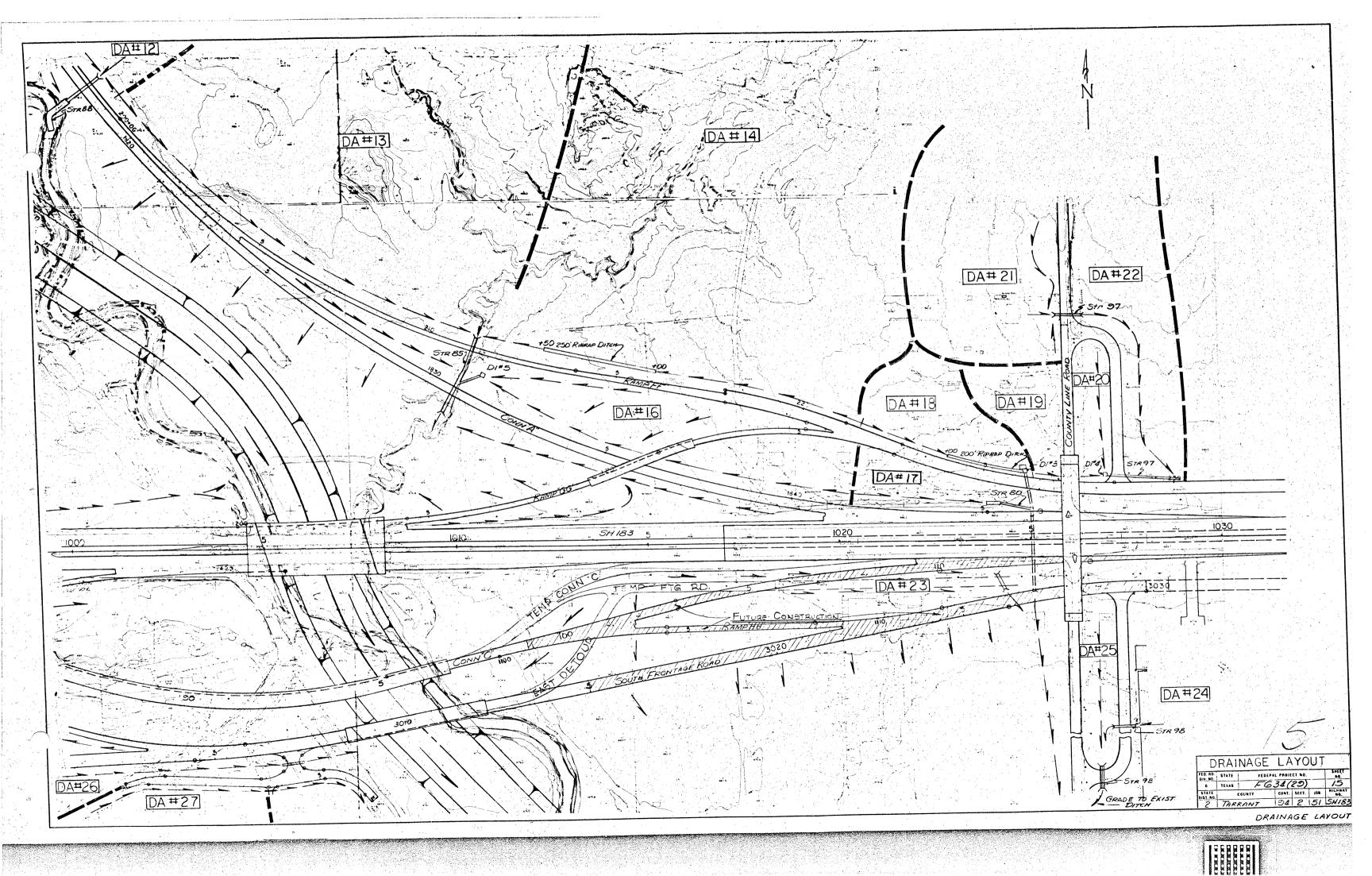


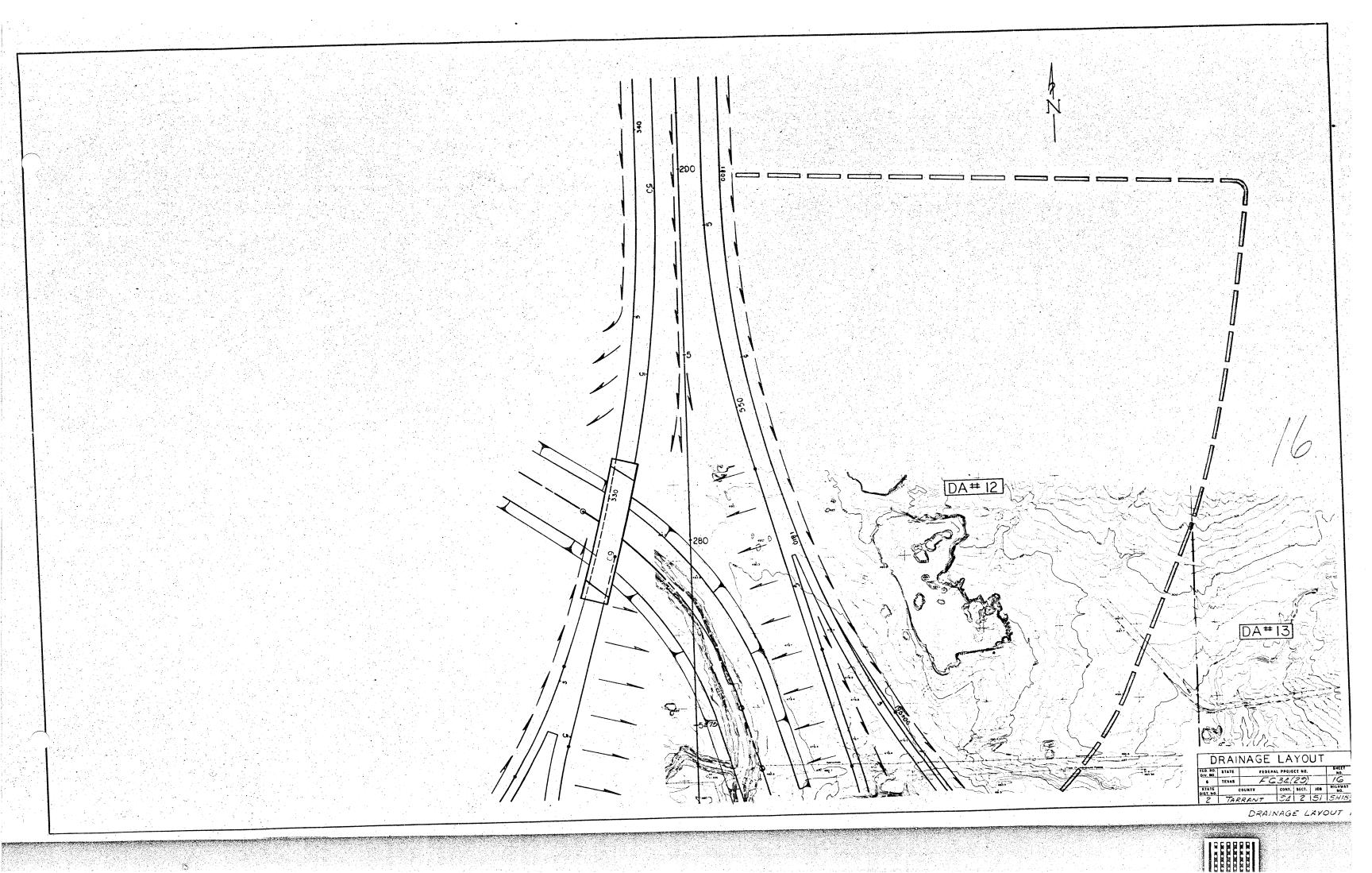
HYDRAULIC DATA

DIN NO	51411			SHEET ND.								
6	18248	11-6	4-634(27)									
STATE DIST NO		COUNTY	CONT.	BECT.	108	PILHUAT NO.						
73	50	1165	192	З	36	F- 163						

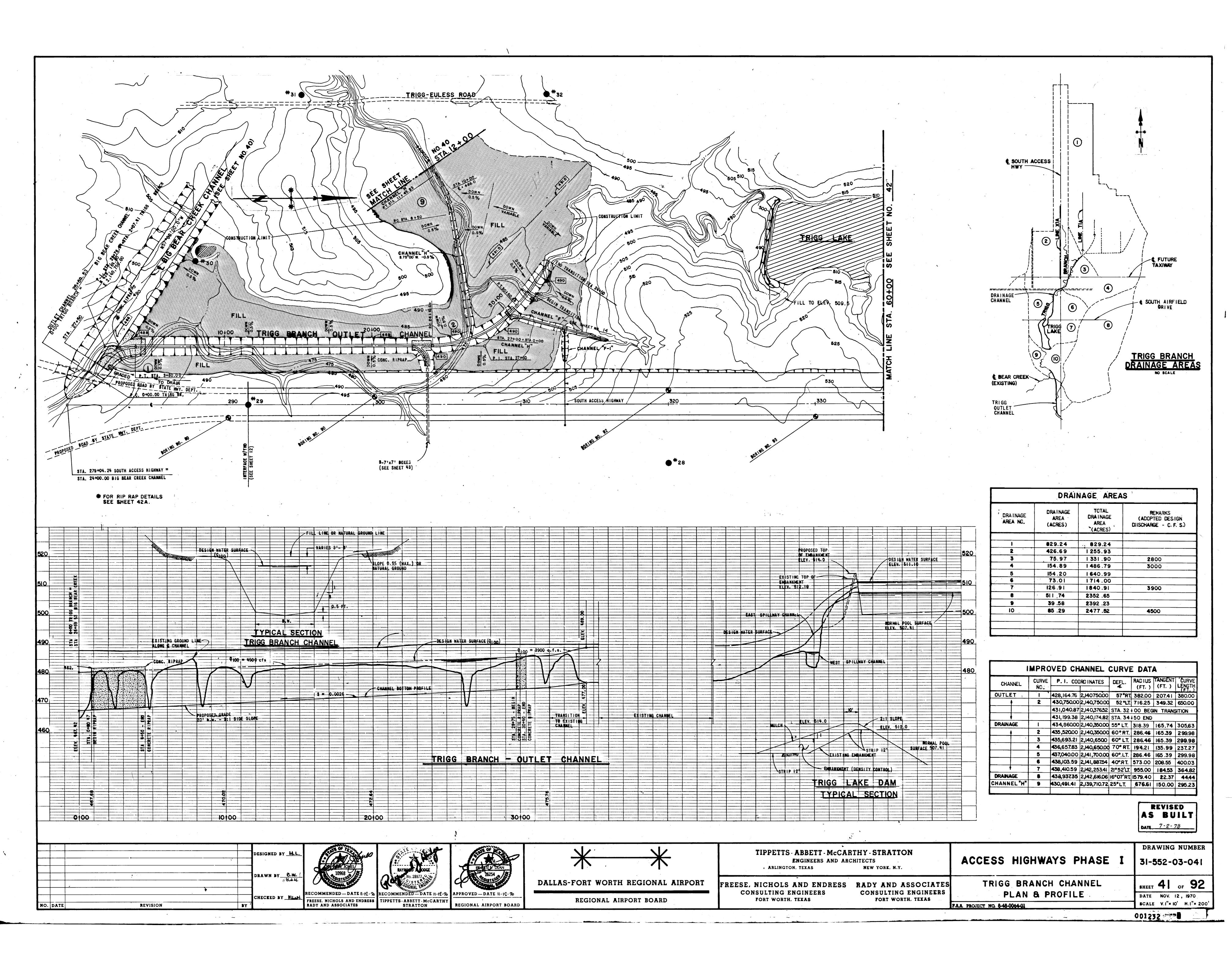


State Highway 183 (Irving)





International Parkway



Appendix D

Digital Data

- HEC-HMS Model
- HEC-RAS Model
- GIS Supporting Data
- Digital Copy of Report

pkce.com

DALLAS 7557 Rambler Rd Suite 1400 Dallas, TX 75231 972.235.3031

FORT WORTH 6100 Western Place Suite 1001

Fort Worth, TX 76107 817.412.7155

HOUSTON 20445 State Highway 249 Suite 380

Houston, TX 77070 281.883.0103